

APPLICATIONS OF THERMODYNAMIC DATABASE FOR REFRACTORIES - STEELMAKING -

Steelmaking Chemistry

The important chemical systems of non-metallic phases for steelmaking processes can be summarized as follows. All of these are modeled in the FactSage databases.

1) Molten slag for refining process

- a) $\text{CaO-FeO-Fe}_2\text{O}_3\text{-SiO}_2\text{-MgO-MnO-P}_2\text{O}_5$ system: BOF process
- b) $\text{CaO-MgO-Al}_2\text{O}_3\text{-SiO}_2\text{-FeO-Fe}_2\text{O}_3$ system: ladle refining process
- c) $\text{CaO-MgO-SiO}_2\text{-CaF}_2$ system: stainless steel refining
- d) $\text{CaO-CrO-Cr}_2\text{O}_3\text{-MgO-SiO}_2$ system: AOD and VOD process for stainless steel
- e) $\text{CaO-MgO-SiO}_2\text{-MnO-CrO-Cr}_2\text{O}_3$ system: high Mn stainless steel

2) Mould flux for casting process

- a) $\text{CaO-MgO-Al}_2\text{O}_3\text{-SiO}_2\text{-Na}_2\text{O-Li}_2\text{O-F}$ system: conventional process
- b) $\text{CaO-MgO-Al}_2\text{O}_3\text{-SiO}_2\text{-Na}_2\text{O-Li}_2\text{O-B}_2\text{O}_3$ system: new candidate.

3) Non-metallic inclusions

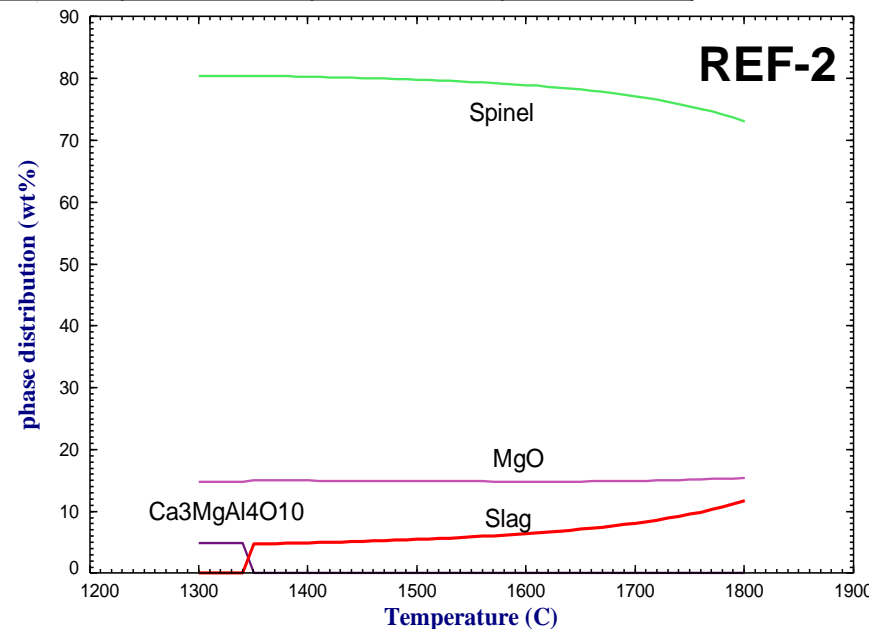
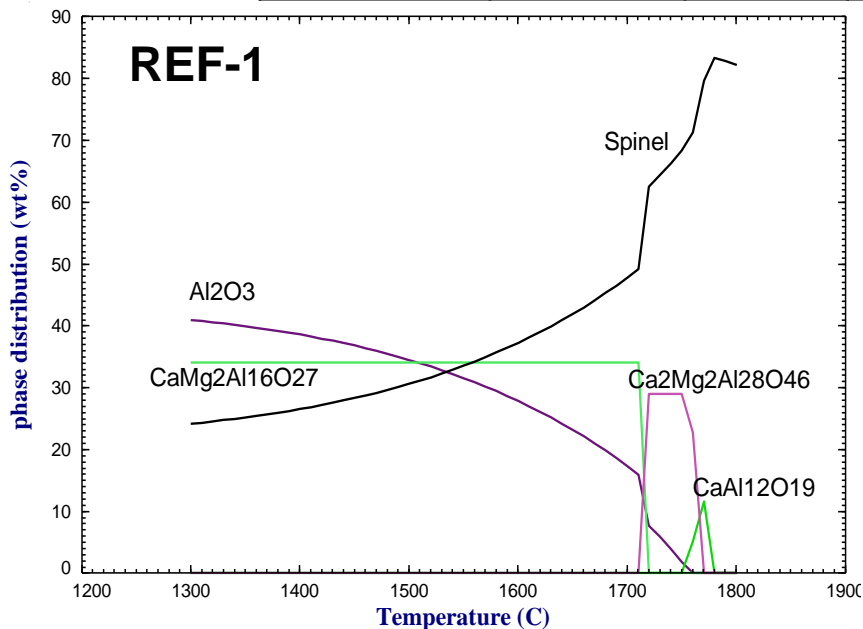
- a) $\text{CaO-Al}_2\text{O}_3\text{-MgO-CaS}$: conventional low carbon steels
- b) $\text{MnO-SiO}_2\text{-Al}_2\text{O}_3\text{-CaO-MnS}$: wire steels and free cutting steels
- c) $\text{MnO-SiO}_2\text{-Ti}_2\text{O}_3\text{-TiO}_2\text{-Al}_2\text{O}_3$: high strength steels
- d) $\text{Al}_2\text{O}_3\text{-Ti}_2\text{O}_3\text{-TiO}_2$: interstitial Free (IF) steels
- e) Ti-Nb-C-N : high-strength low-alloy (HSLA) steels containing Ti and Nb

4) Refractories

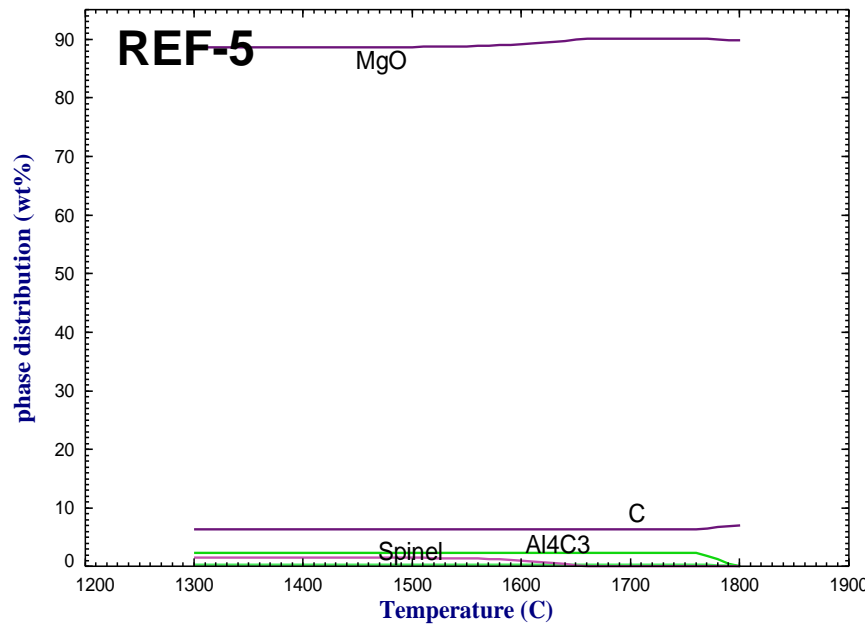
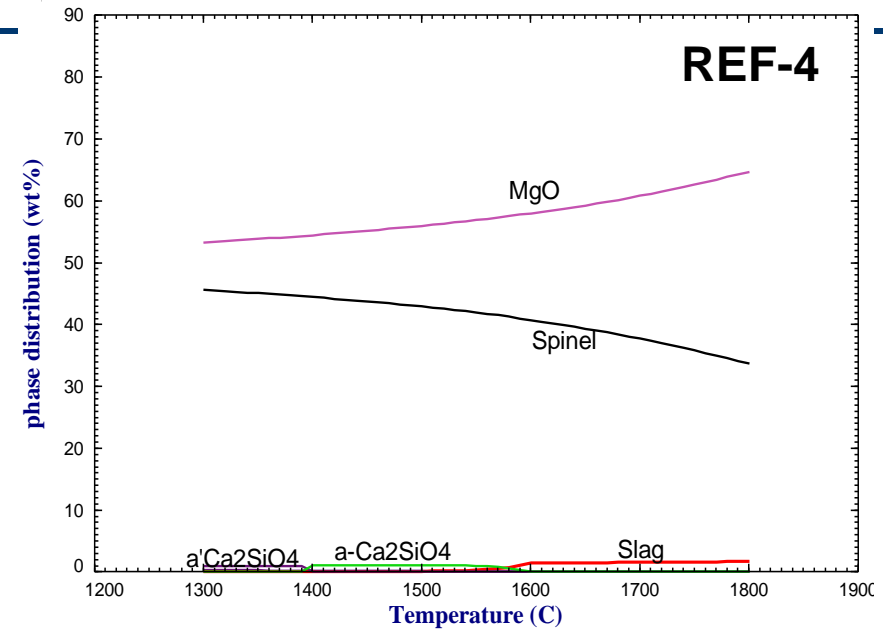
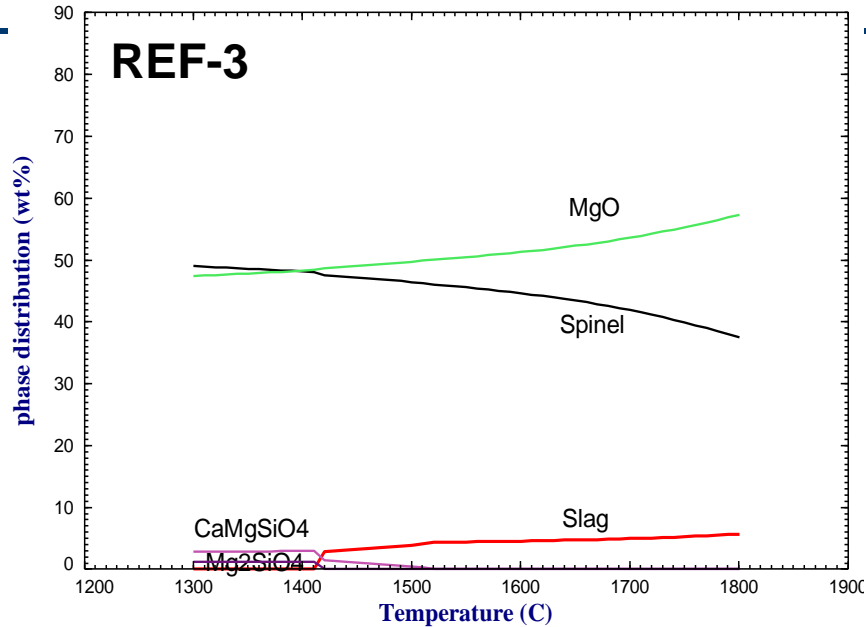
- a) MgO-C : BOF and RH vessel refractories, ladle slag line
- b) $\text{MgO-Al}_2\text{O}_3$: ladle castable
- c) $\text{MgO-Cr}_2\text{O}_3\text{-FeO-Fe}_2\text{O}_3\text{-Al}_2\text{O}_3$: VOD and AOD refractories
- d) $\text{Al}_2\text{O}_3\text{-ZrO}_2\text{-SiO}_2\text{-C}$: nozzle refractories and tundish plugs

Thermal Stability test of RH refractories

wt%	REF-1	2	3	4	5	6
Al_2O_3	88	60	11	4	0.5	0.5
MgO	9	38	58	61	89	75
CaO	2	2	0.9	0.7		
Cr_2O_3			20	29		
Fe_2O_3			8.8	4.8		
SiO_2			1.6	0.4	0.5	1.2
C					7	17
Al					2	4



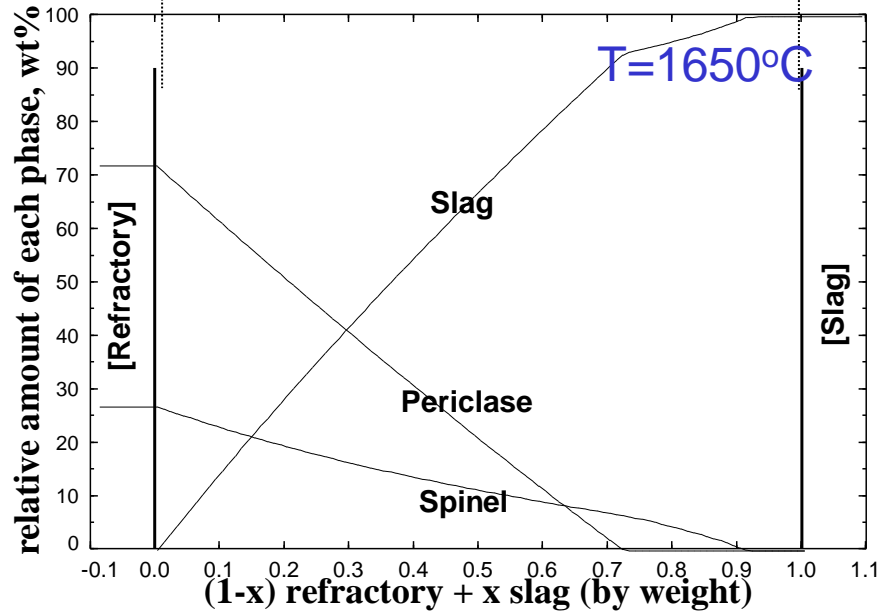
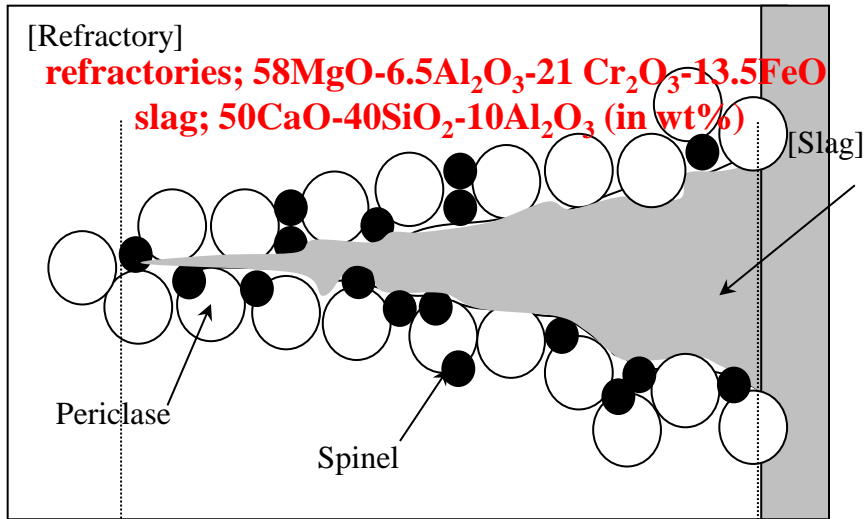
Stability test of RH refractories



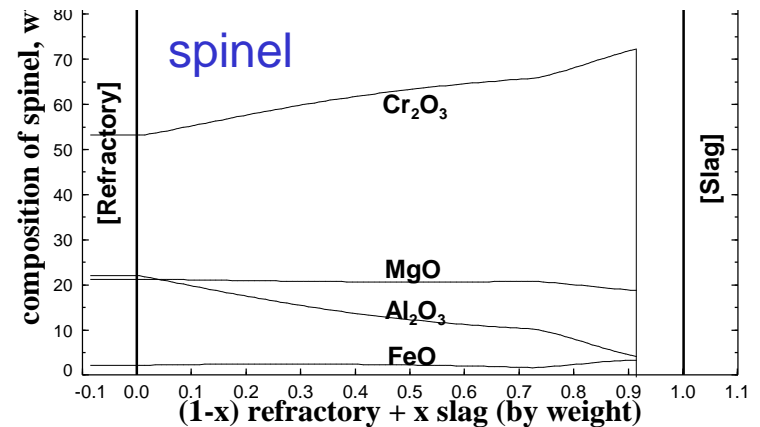
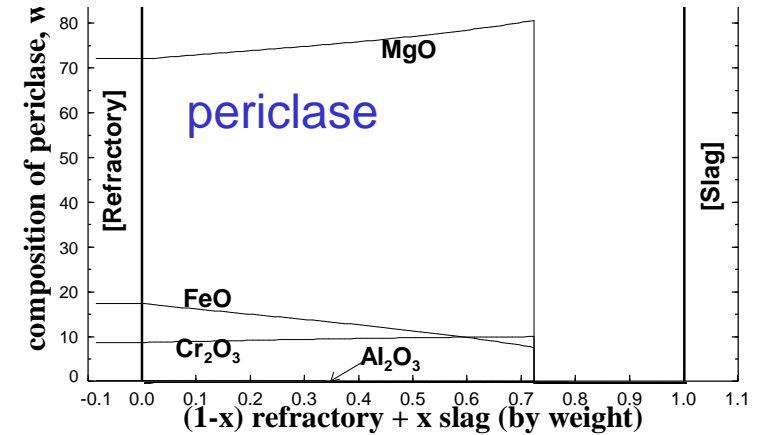
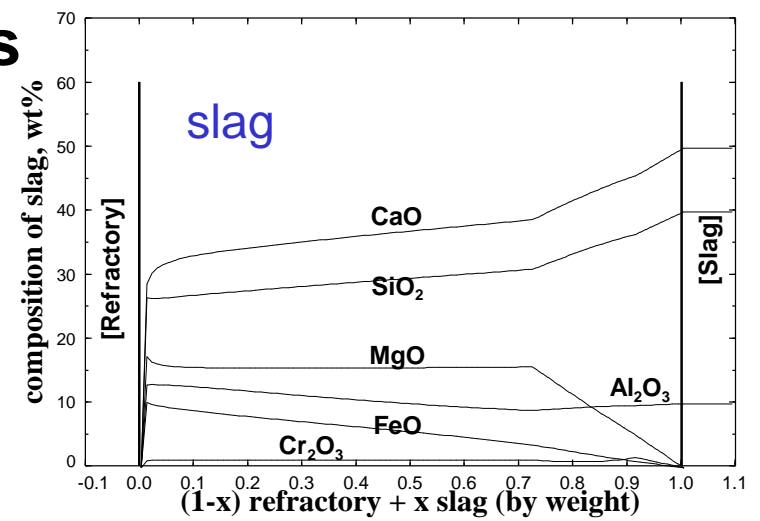
Depending on the refractory compositions, the refractory components can vary drastically.

- Formation of liquid
 - Stability of refractory ↓
- Change in MgO/Spinel fraction
 - Mechanical wear resistance
 - Volume change

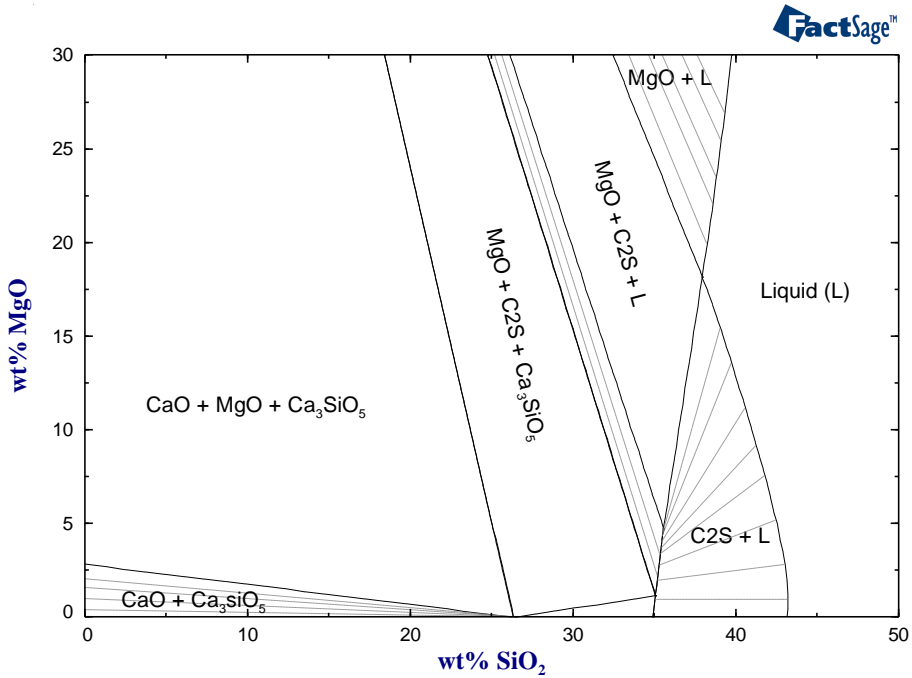
Refractory/Slag rxn in VOD process



Jung et al., *Taikabutsu*, vol. 56, 2004, pp. 382-386.

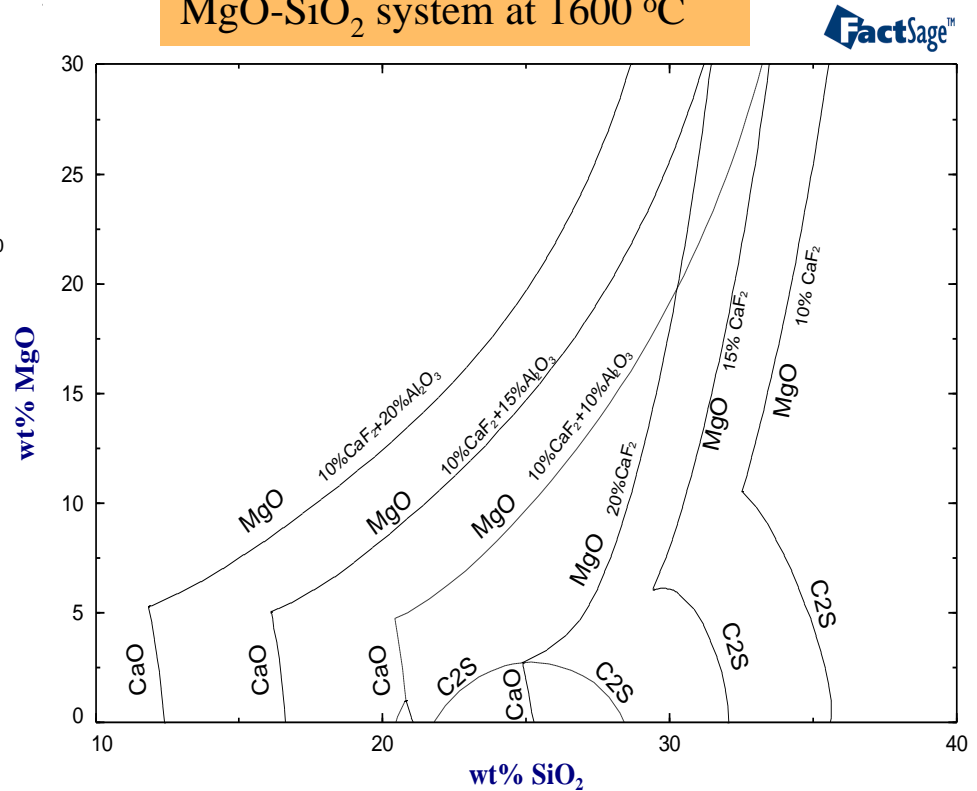


Refractory reaction with F-containing slag/flux



Phase diagram of the CaO-MgO-SiO₂ system at 1600 °C

Influences of CaF₂ and Al₂O₃ on the liquidus of the CaO-MgO-SiO₂ system at 1600 °C



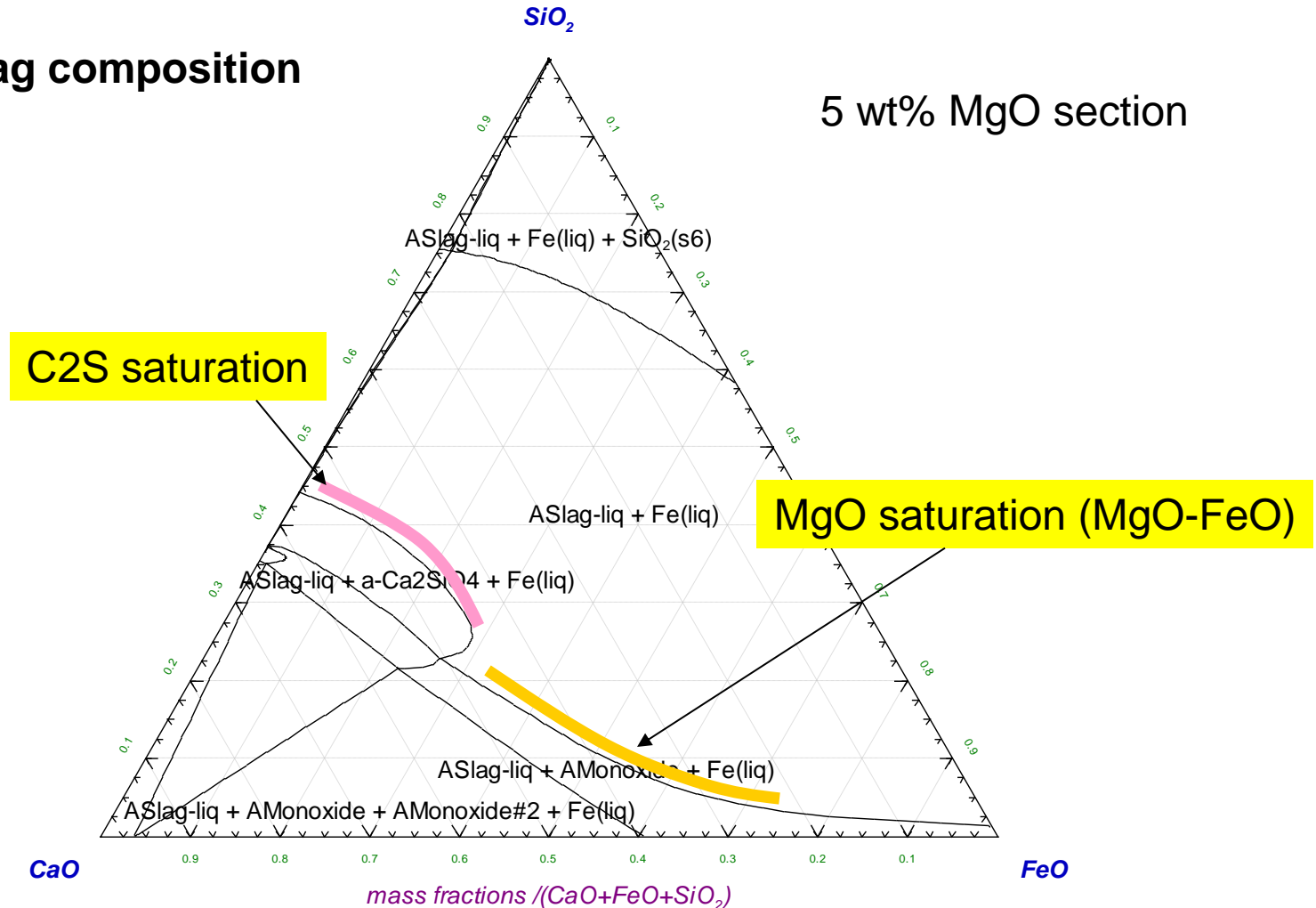
Refractory: CaO-Fe_tO-SiO₂-5wt%MgO system with Fe saturation

CaO - FeO - SiO₂ - MgO - Fe
1650°C, MgO/Z (g/g) = 0.05263, Fe/Z (g/g) = 0.001,
Z=(CaO+FeO+SiO₂)



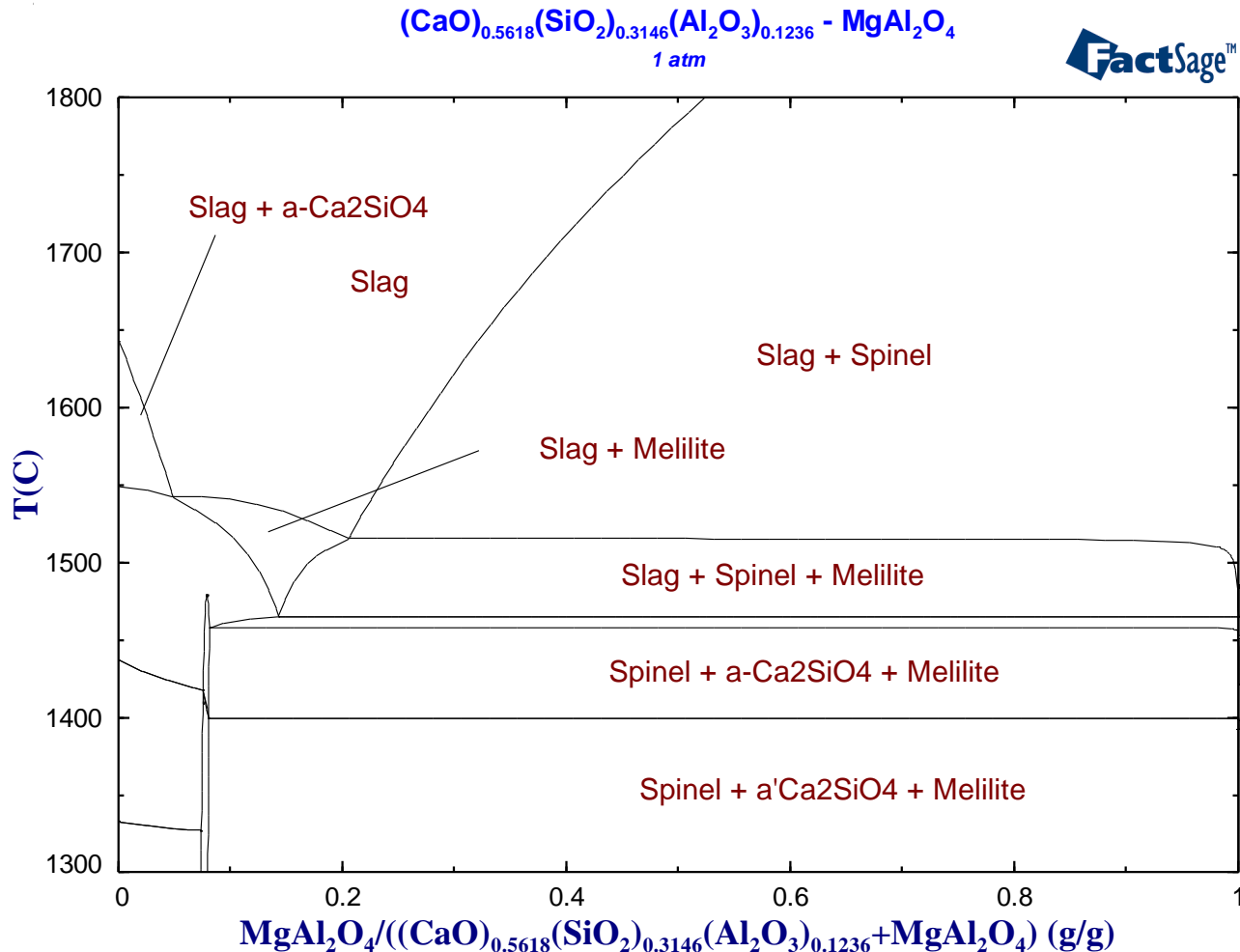
BOF slag composition

5 wt% MgO section



CaO-Al₂O₃-SiO₂ slag – MgAl₂O₄ refractory

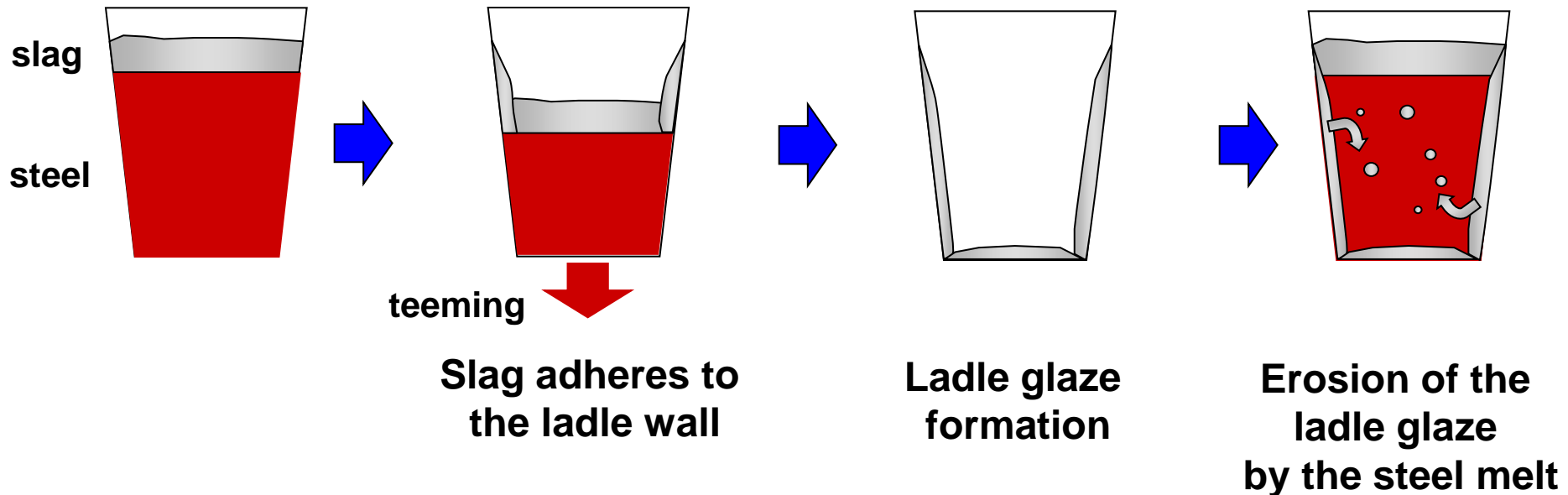
50%CaO-30%SiO₂-20%Al₂O₃ slag → in mole: (CaO)_{0.5618}(SiO₂)_{0.3146}(Al₂O₃)_{0.1236}
(Equilib or Phase Diagram's components are in molar base)



Ladle Glaze ??

Ladle Glaze

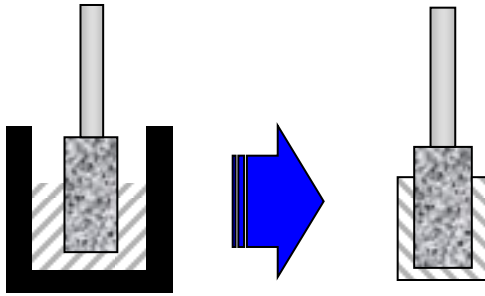
- Reactions with Ladle refractory lining
- Formation of non-metallic Inclusions



Purpose of the present study

- Glaze formation mechanism / Glazed refractory
- Influence on melt cleanliness (inclusion): Al, Al/Ca

Ladle Glaze formation



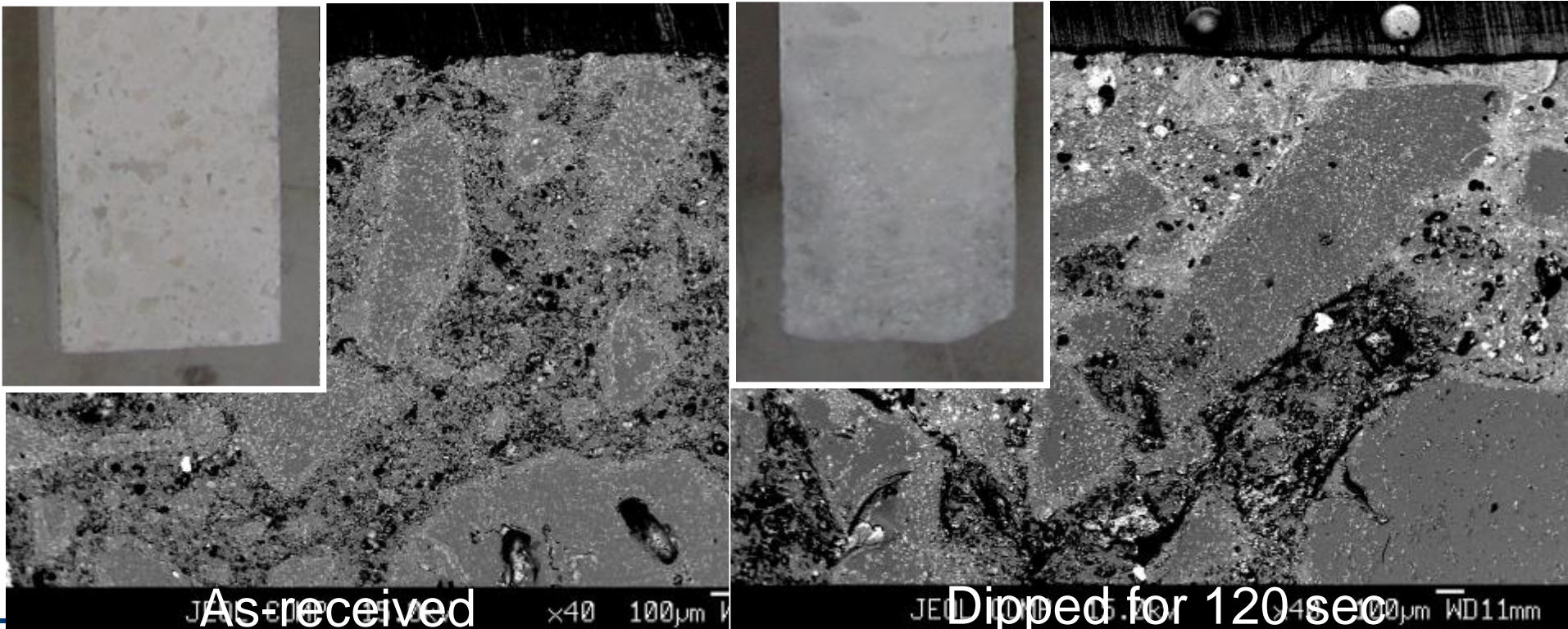
Dipping time: 120 sec

Refractory composition (wt.%)

CaO	SiO ₂	Al ₂ O ₃	MgO
2.35	0.76	88.06	8.35

Slag composition (wt.%)

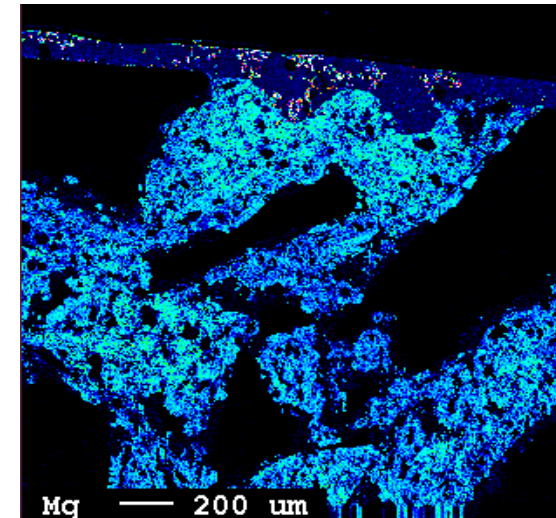
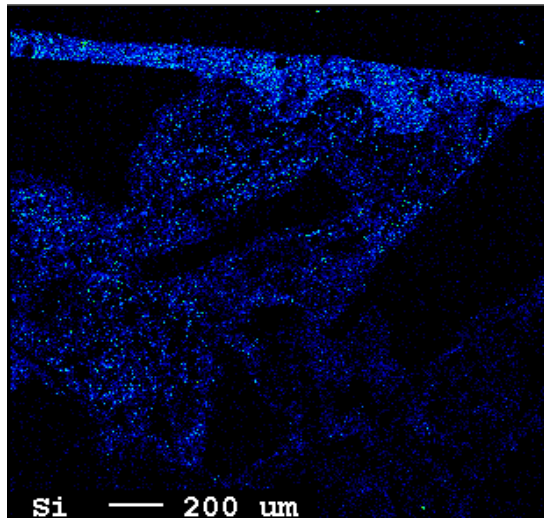
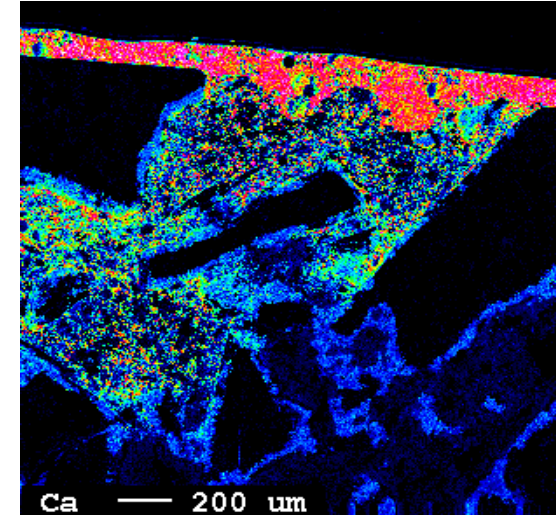
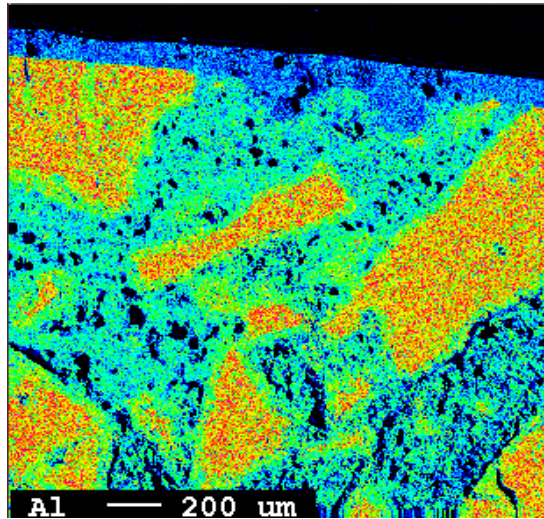
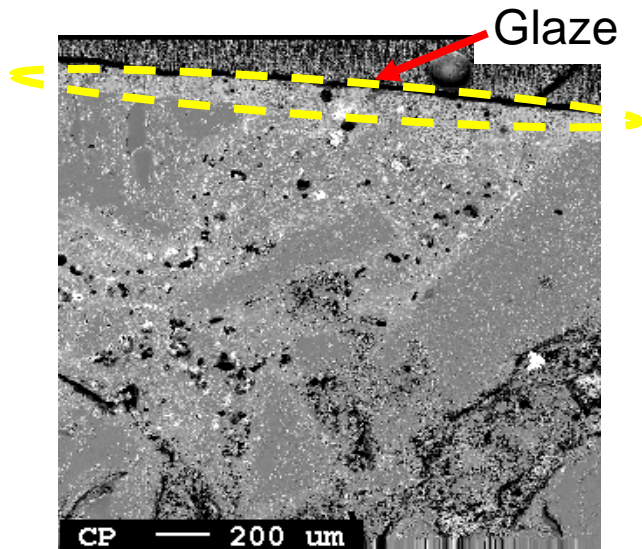
CaO	SiO ₂	Al ₂ O ₃	MgO
54.06	10.47	26.24	9.23



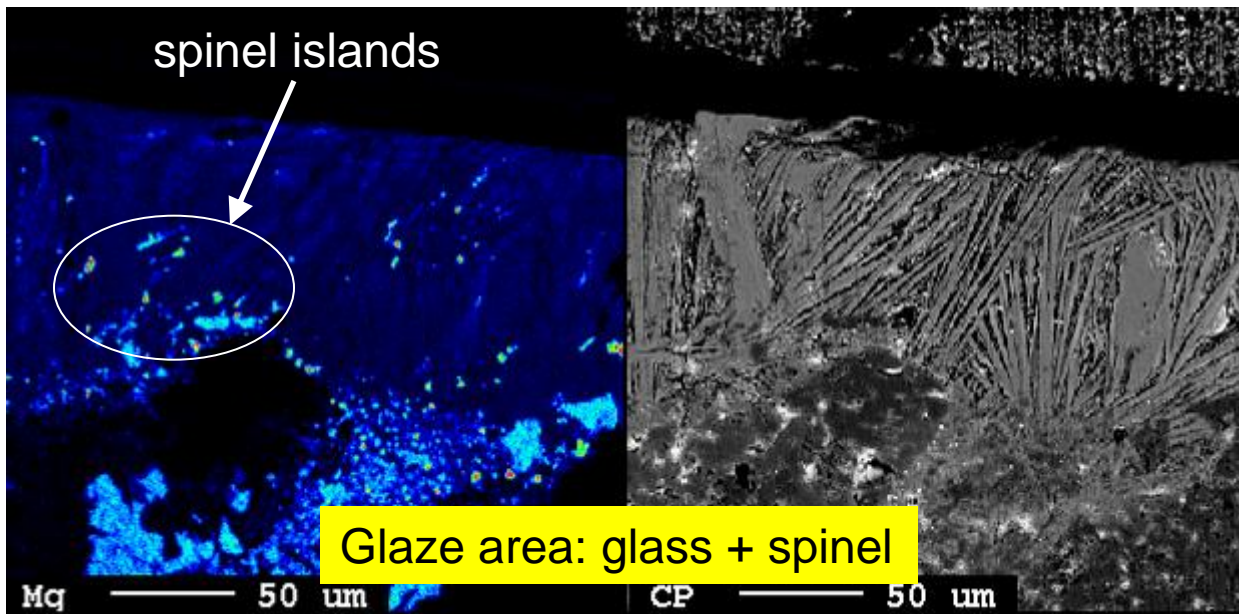
As received

Dipped for 120 sec

Glazed Refractory

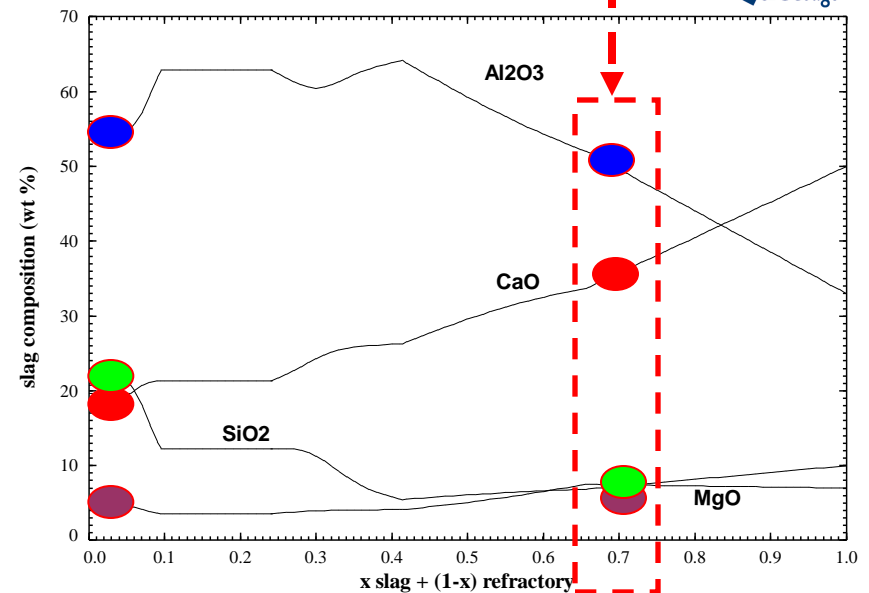
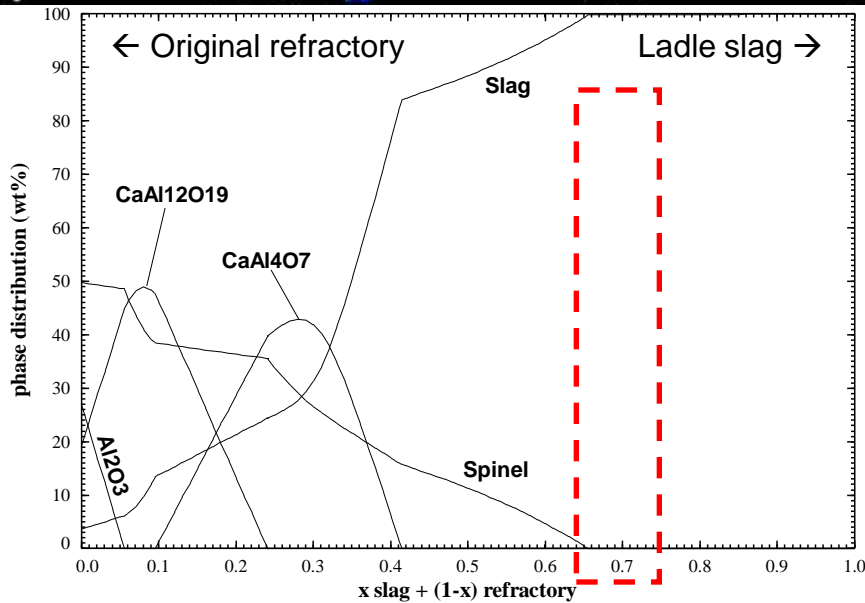


Glaze (Reaction product of slag and refractory)



Glaze composition (glass)

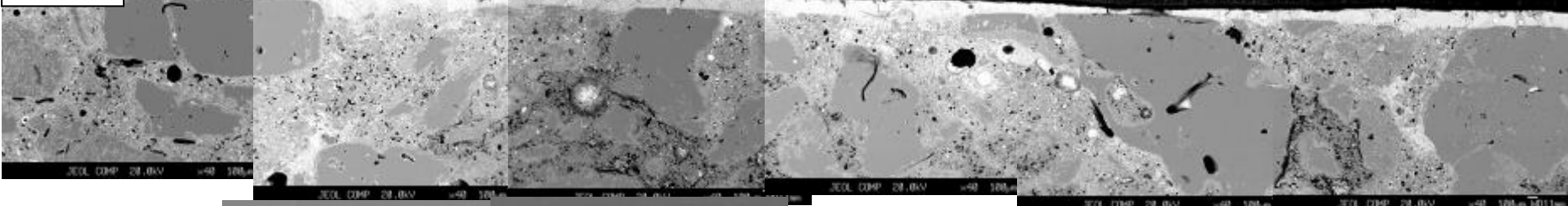
CaO	SiO ₂	Al ₂ O ₃	MgO
35.8	6.6	51.1	6.5



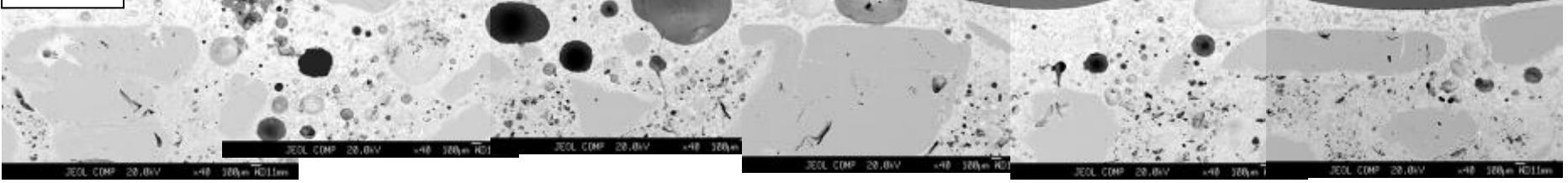
Change of Glazed refractory by chemical reaction with **Al-deoxidized** molten steel

— 500μm

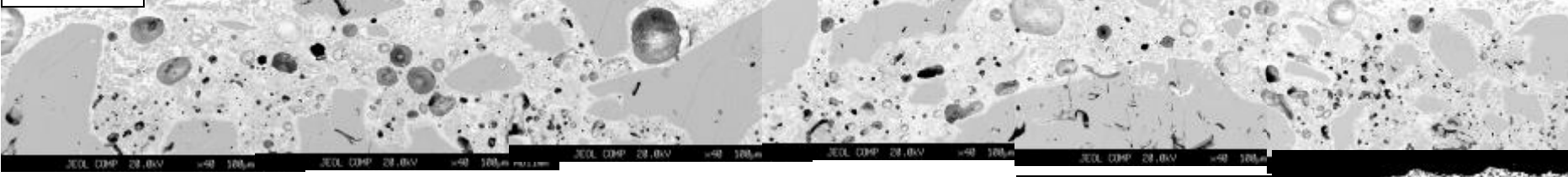
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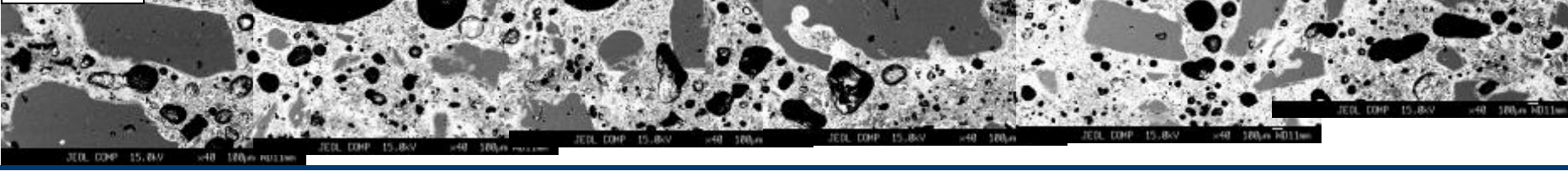
1min



3mins

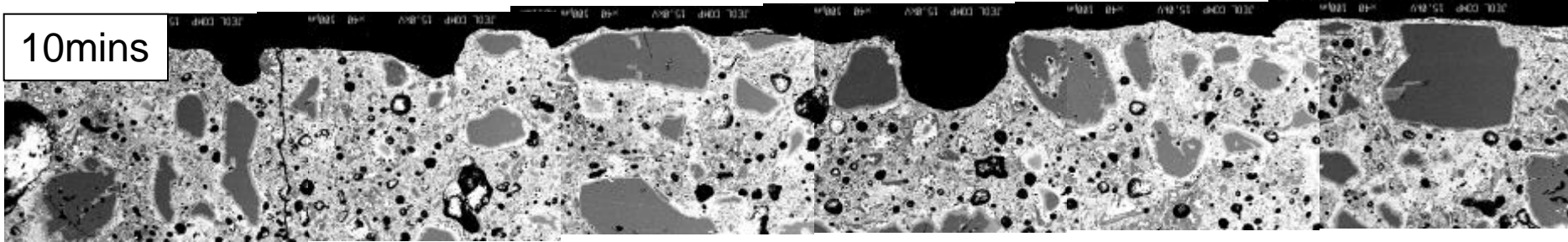


5mins

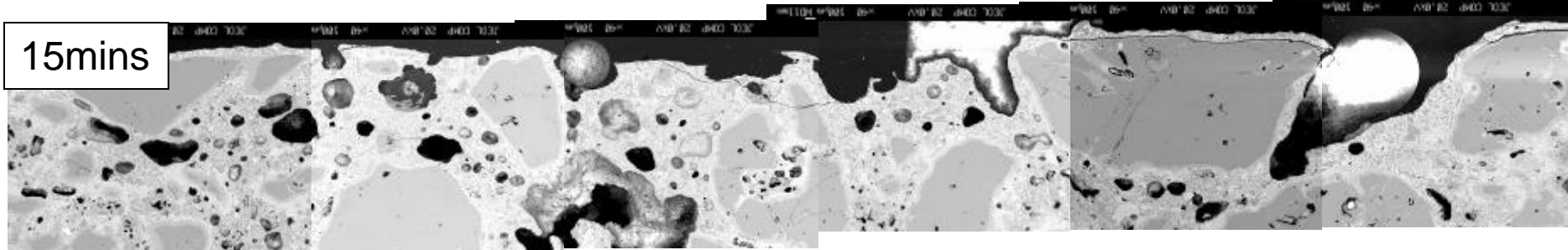


Change of Glazed refractory by chemical reaction with **Al-deoxidized** molten steel

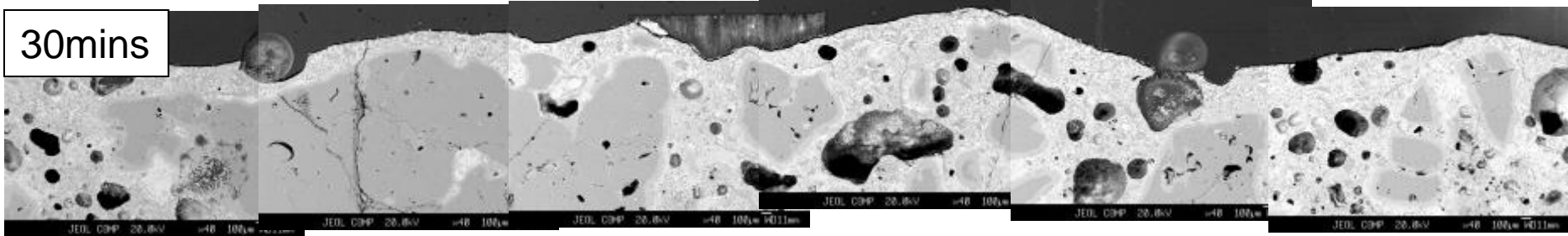
10mins

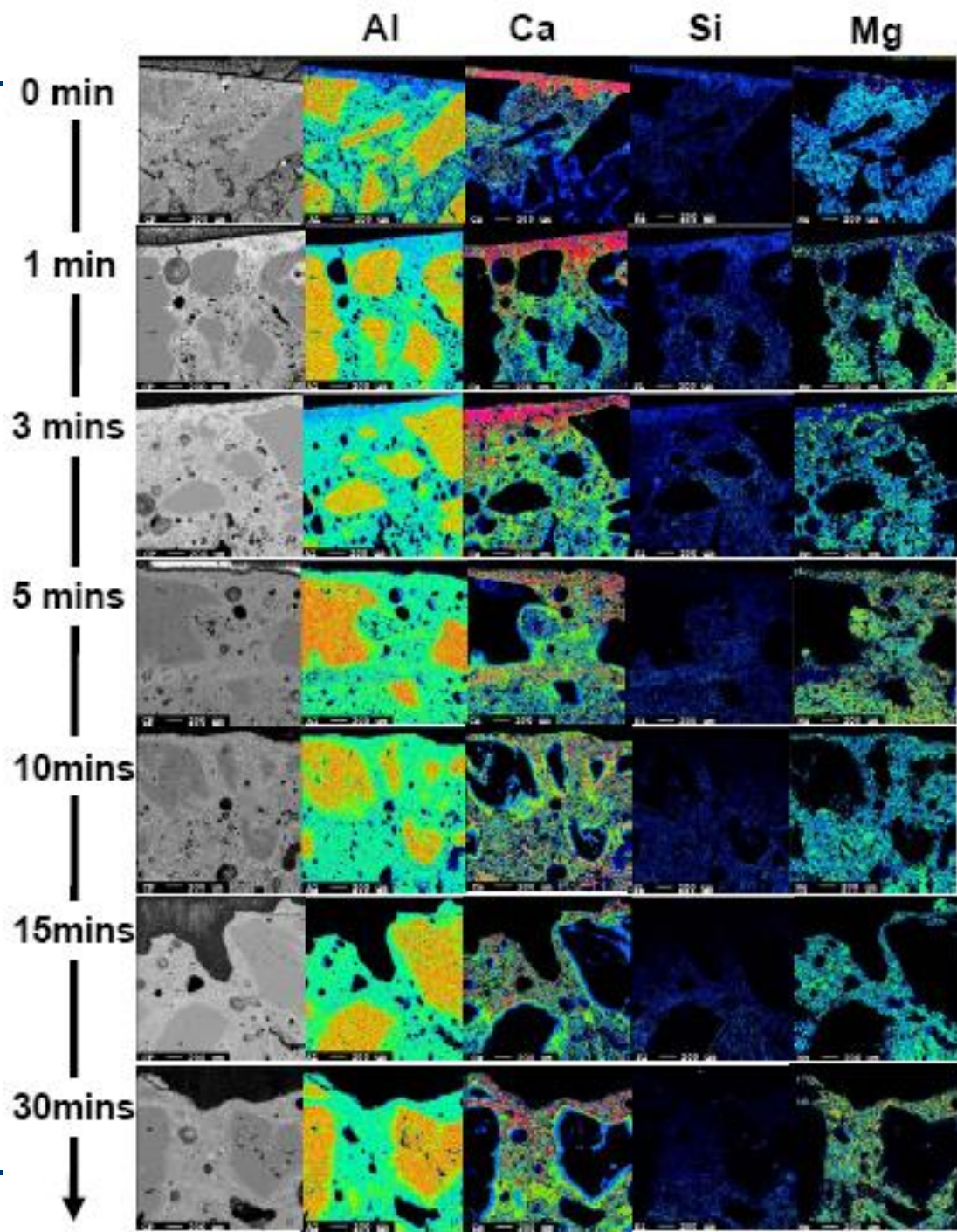


15mins



30mins

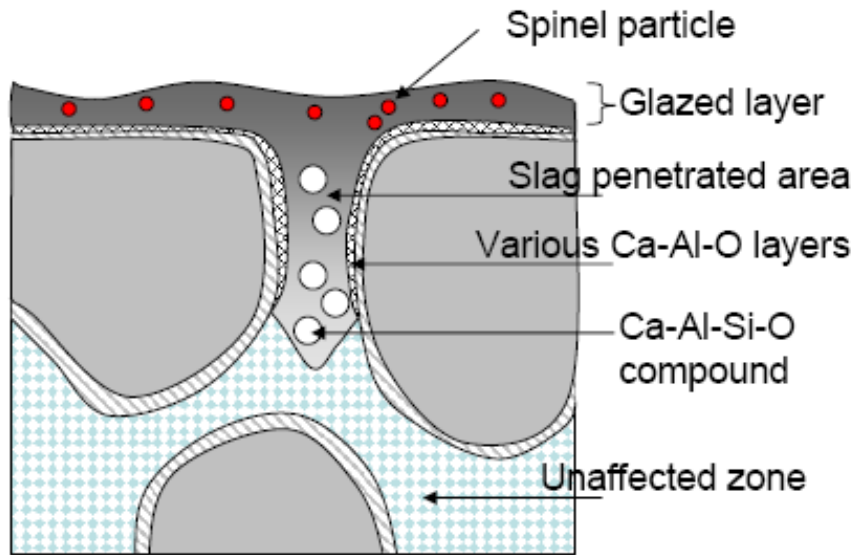




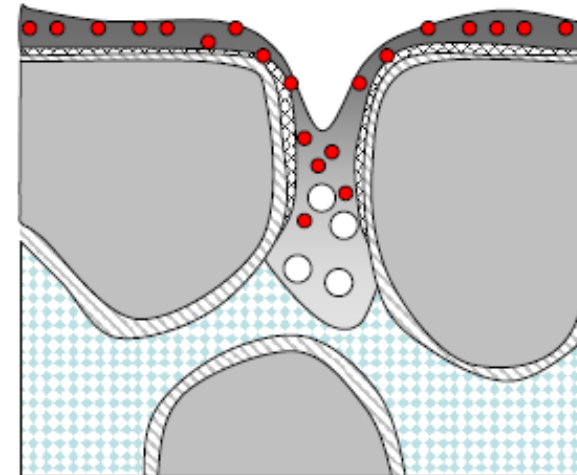
Morphology of Glazed refractory in molten steel (Al-deoxidized)

Penetration of Glaze into refractory (Ca and Si mapping images)

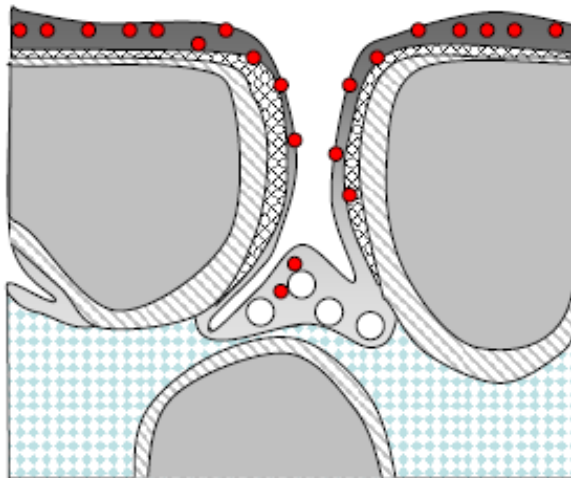
Change of Glazed refractory in Al (Al/Ca) steel



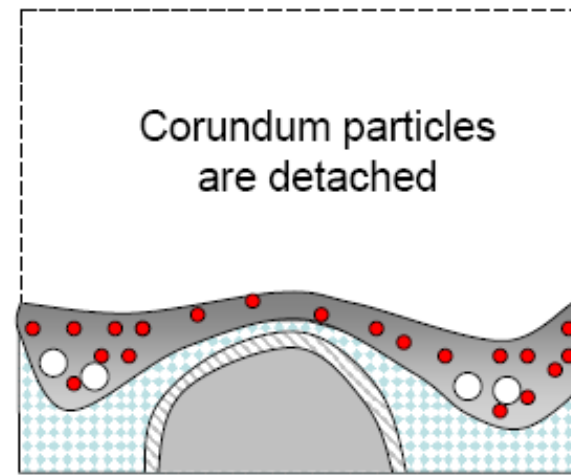
(a)



(b)

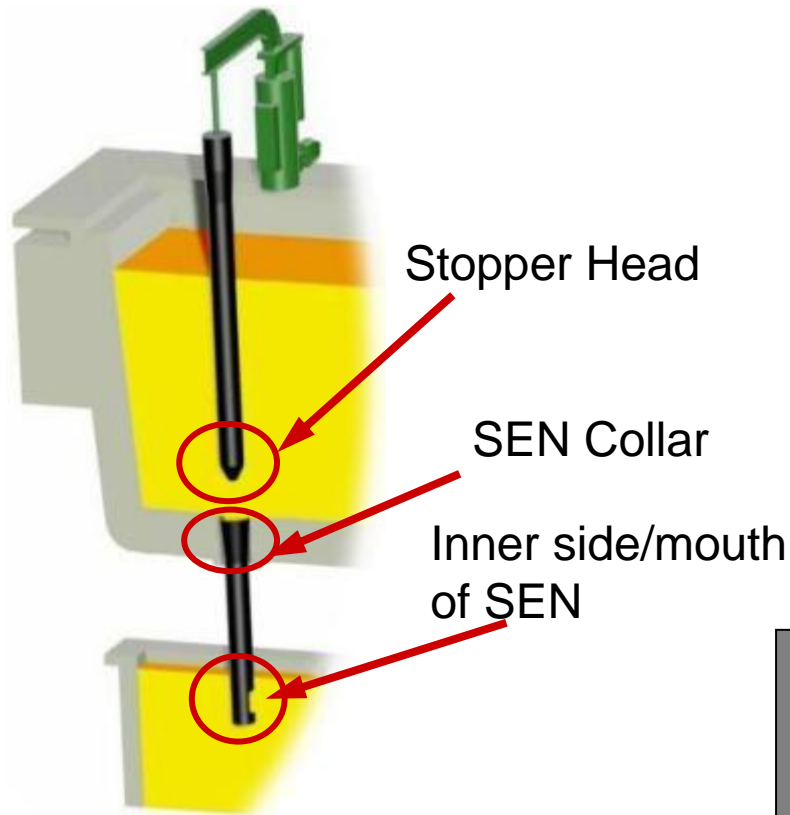


(c)

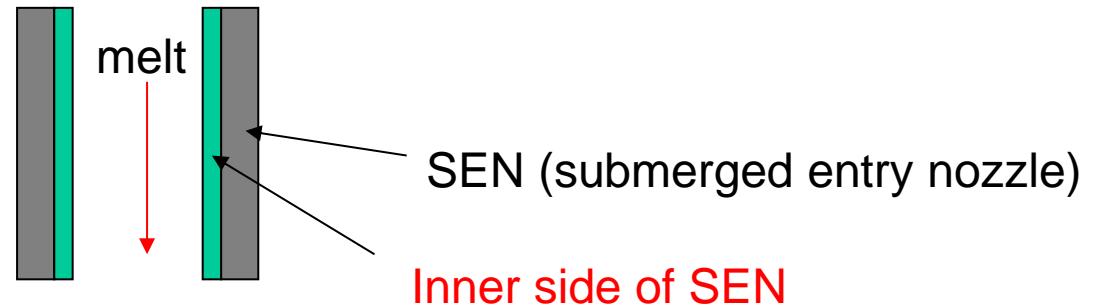
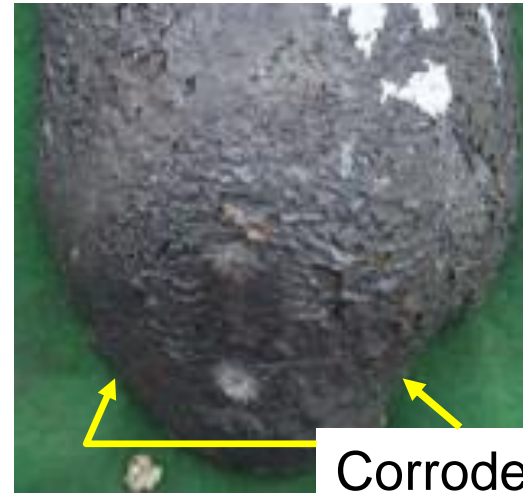


(d)

Refractory – Liquid Inclusion Interactions



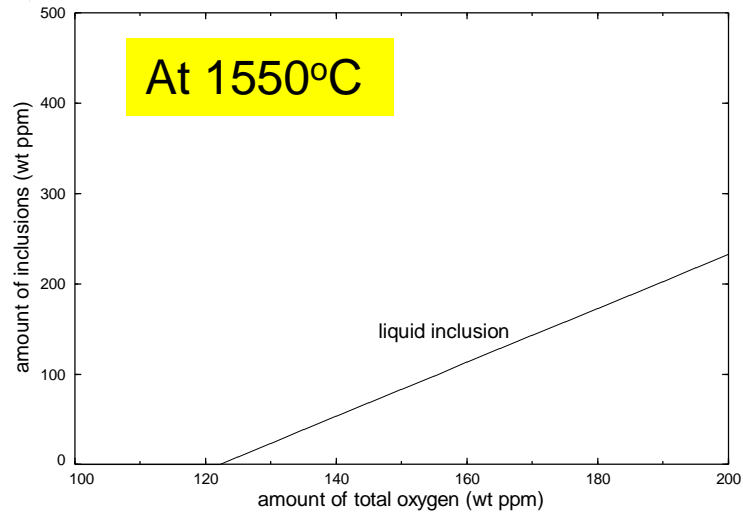
Stopper ($\text{Al}_2\text{O}_3\text{-C}$)



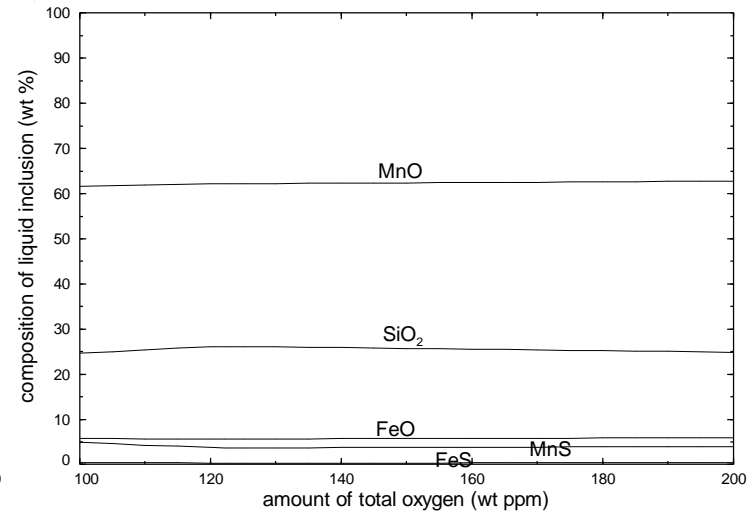
M.-K. Cho and I.-H. Jung, "Corrosion of nozzle refractories by liquid inclusion in high oxygen steels", ISIJ Inter. 2012, vol. 52, pp. 1289-1296.

Refractory – Liquid Inclusion Interactions

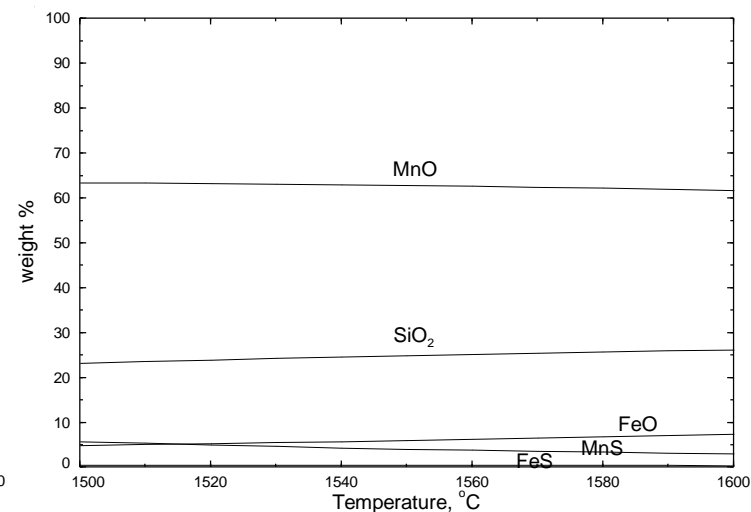
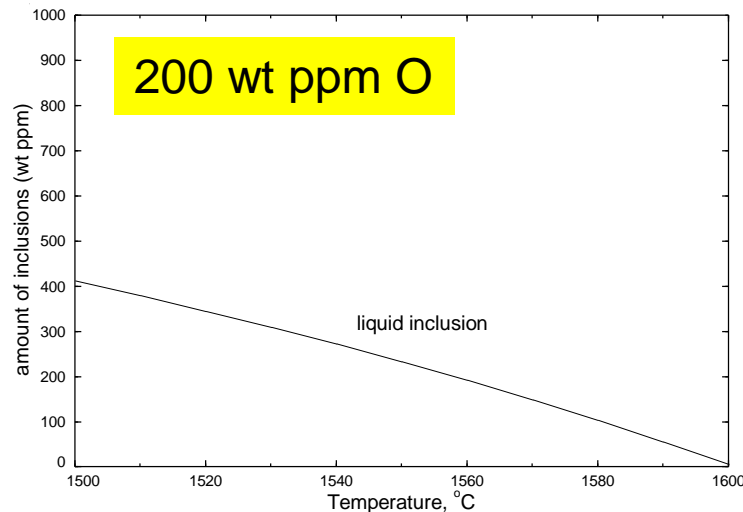
Fe-0.08C-1.2Mn-0.3S-0.01Si-O-minor P, Bi, etc. in wt %



(a)



(b)

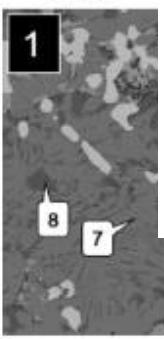
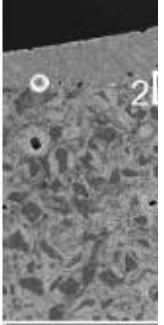


Refractory – Liquid Inclusion Interactions

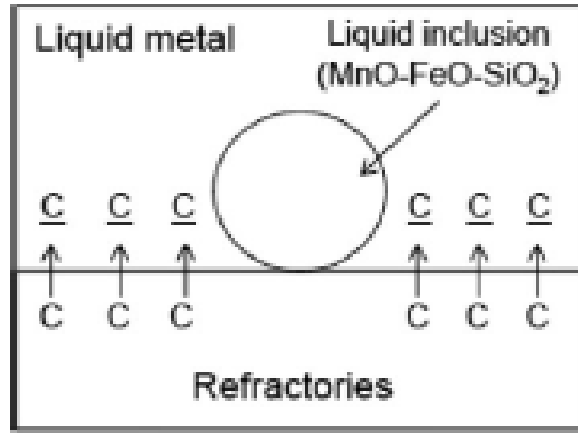
Table 1. Chemical compositions of the refractories investigated in

wt%
Al ₂ O ₃
MgO
ZrO ₂
C

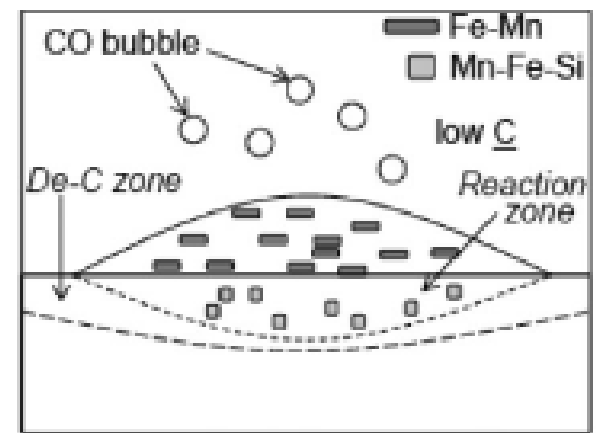
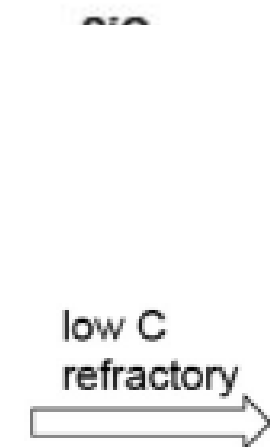
Al₂O₃



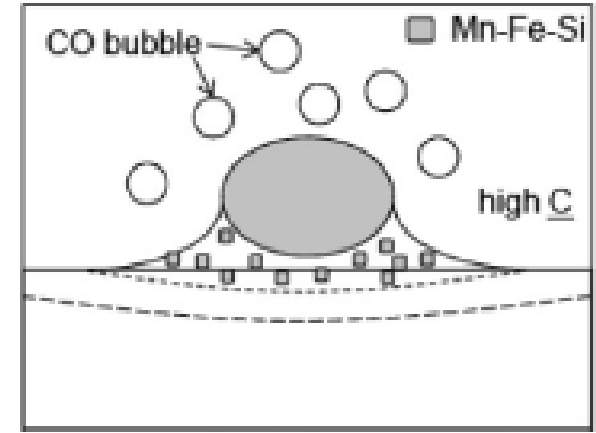
100µm



50µm

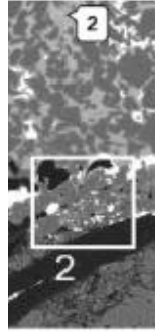


Partial reduction of liquid inclusion, Wetting and Chemical reaction



60µm

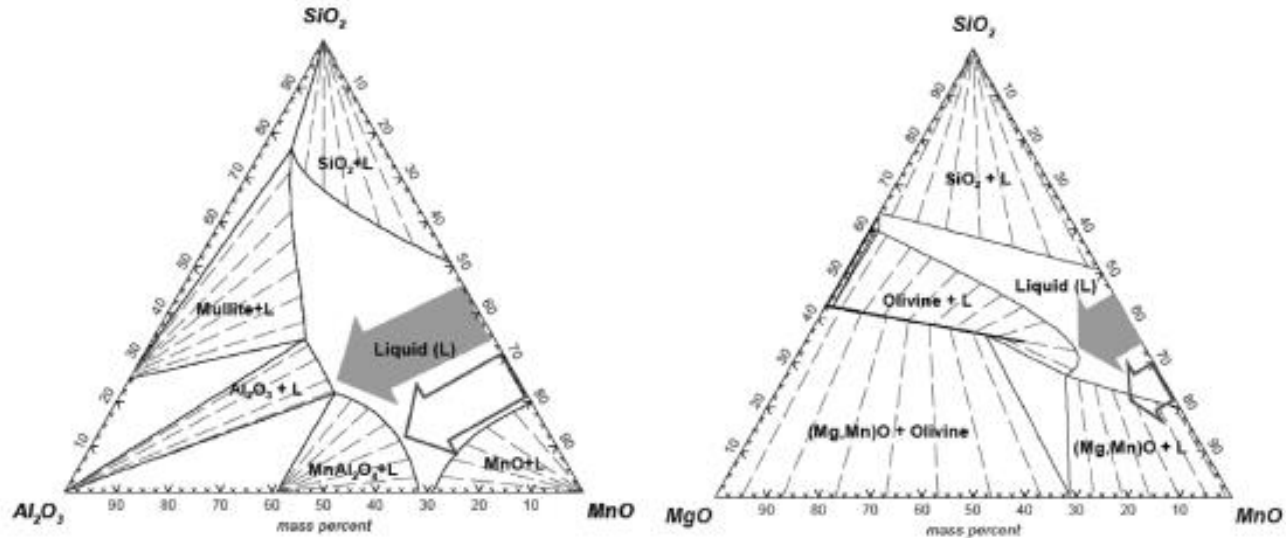
10µm



10µm

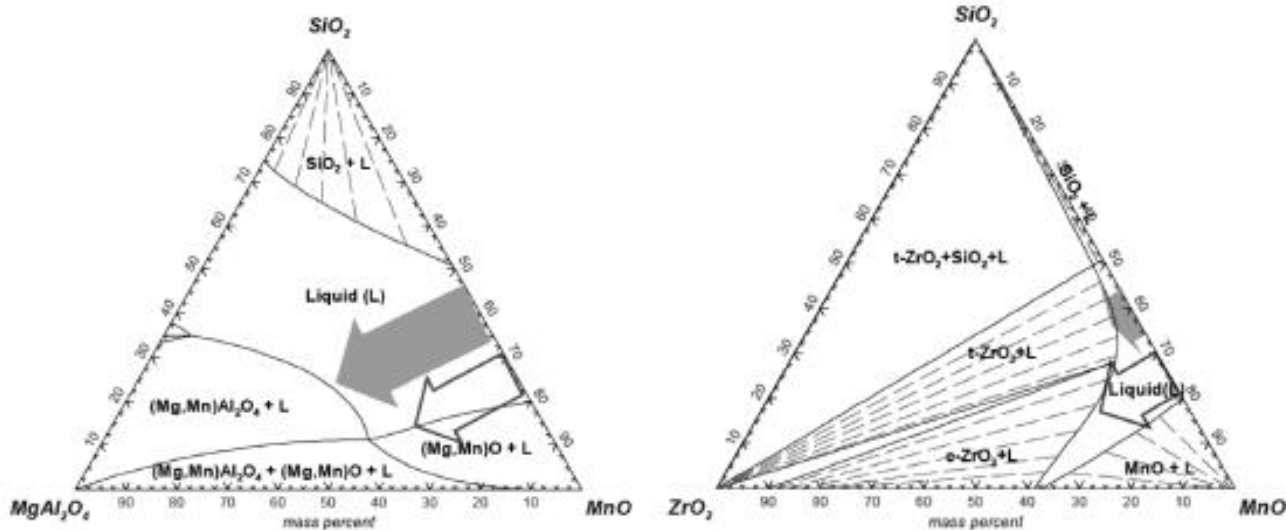
Refractory – Liquid Inclusion Interactions

Relative Stability of the refractories against liquid MnO-SiO₂ type inclusion



(a)

(b)

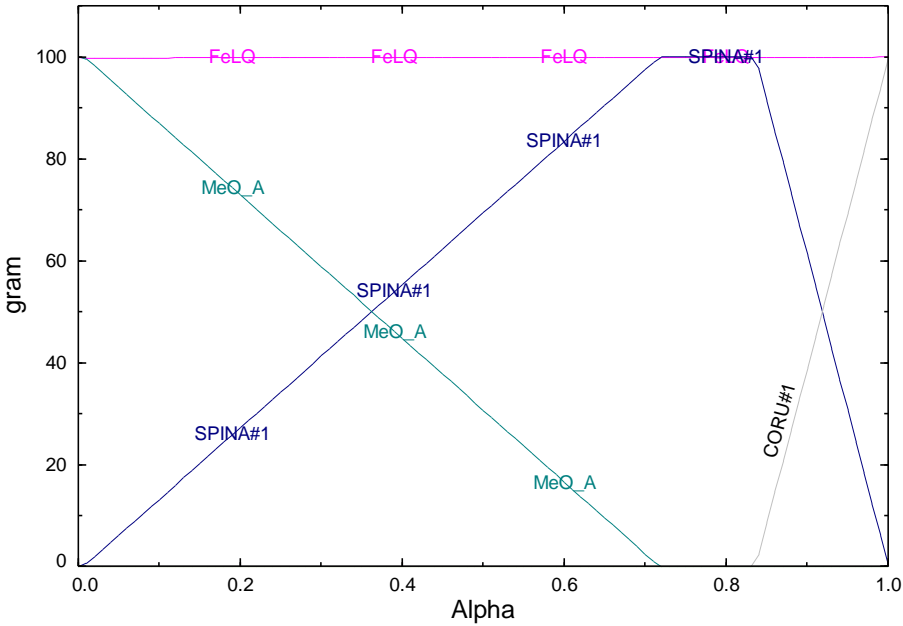


(c)

(d)

Refractory-Steel Interaction

95 Fe + 4 Mn + Si + <100-100A> MgO +
C:\Slag-Steel-Inclusions\Equi0.res 24Sep12

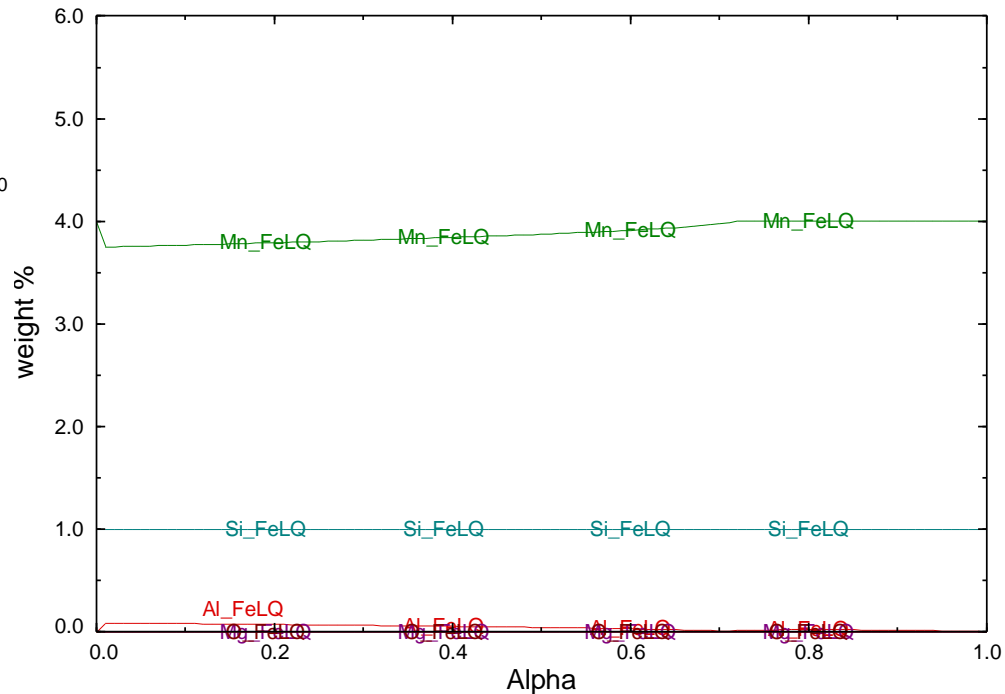


← Change in the amount of phases

<100A> Al₂O₃ + <100-100A> MgO

Change in steel composition →

95 Fe + 4 Mn + Si + <100-100A> MgO +
C:\Slag-Steel-Inclusions\Equi0.res 24Sep12



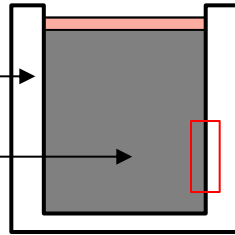
<100A> Al₂O₃ + <100-100A> MgO

High Mn-Fe melt storage for TWIP Steel production

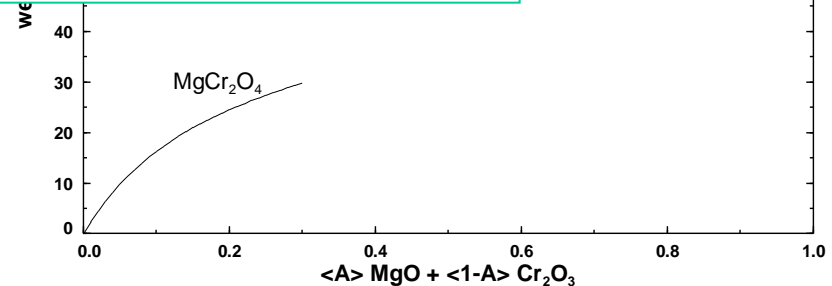
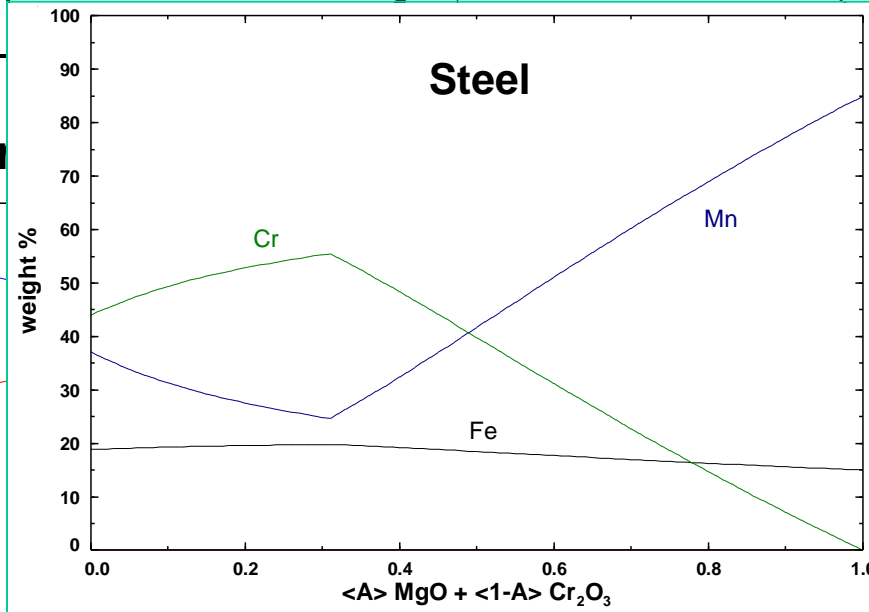
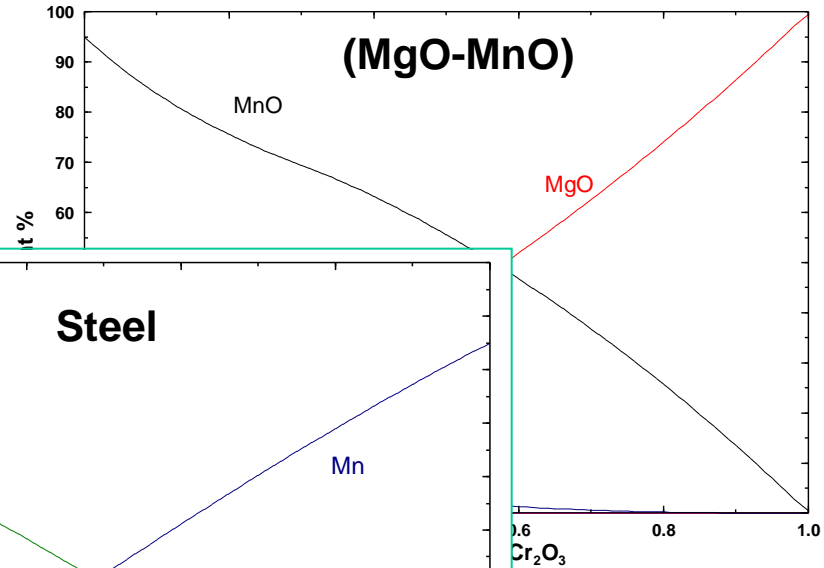
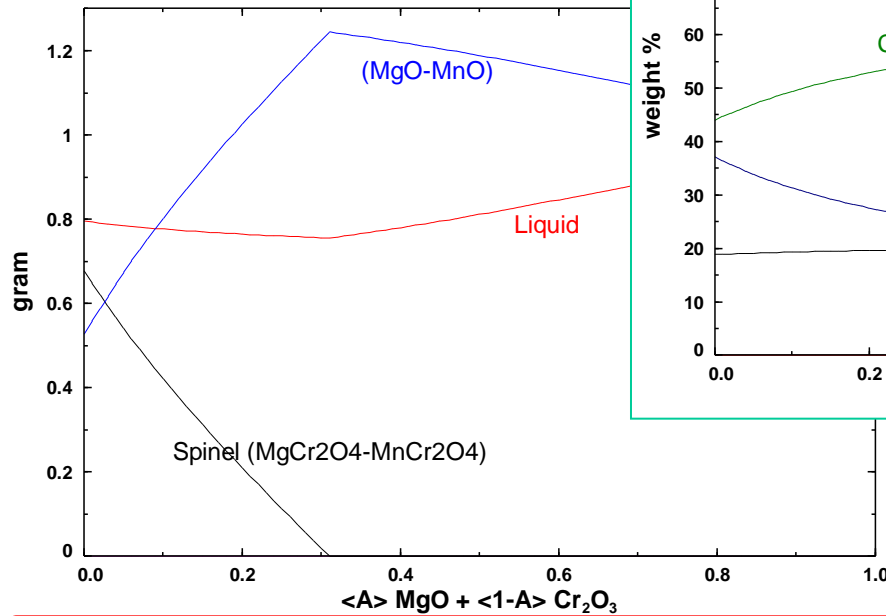
Melt / refractory reactions simulation

Refractories

85%Mn-15%Fe melt

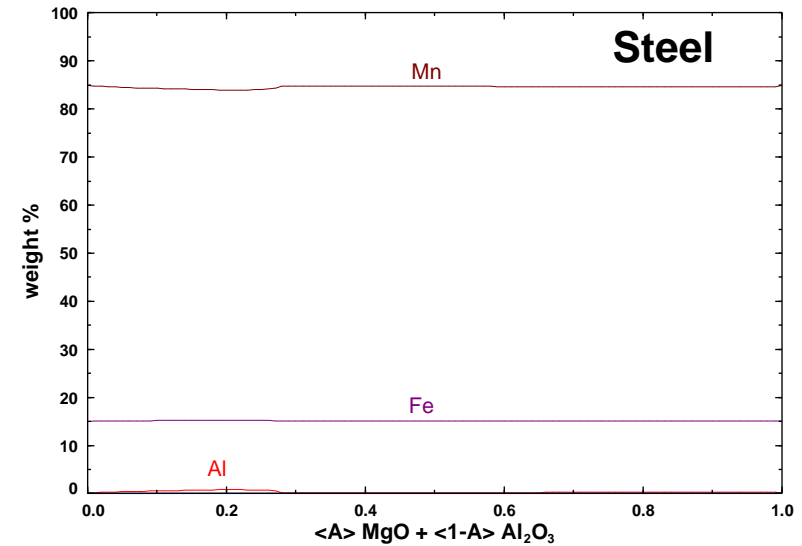
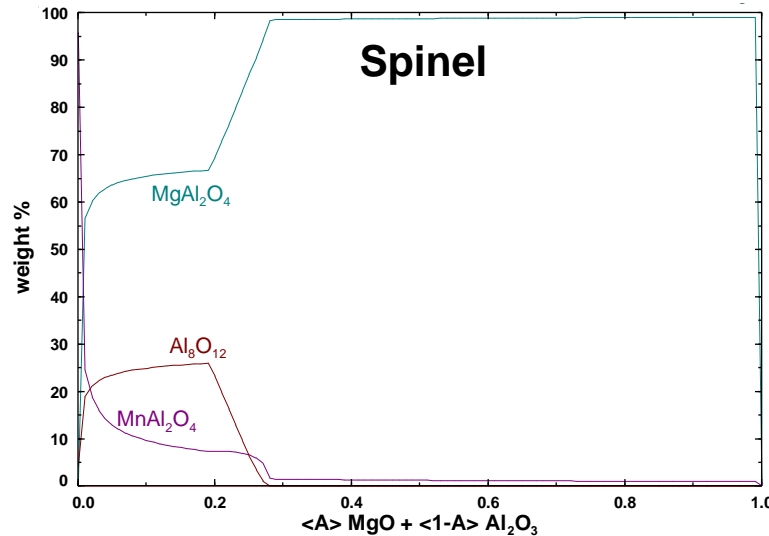
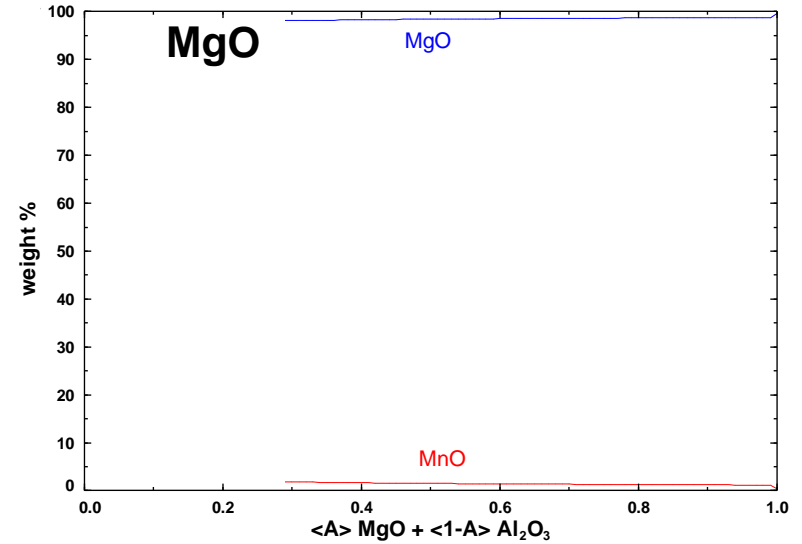
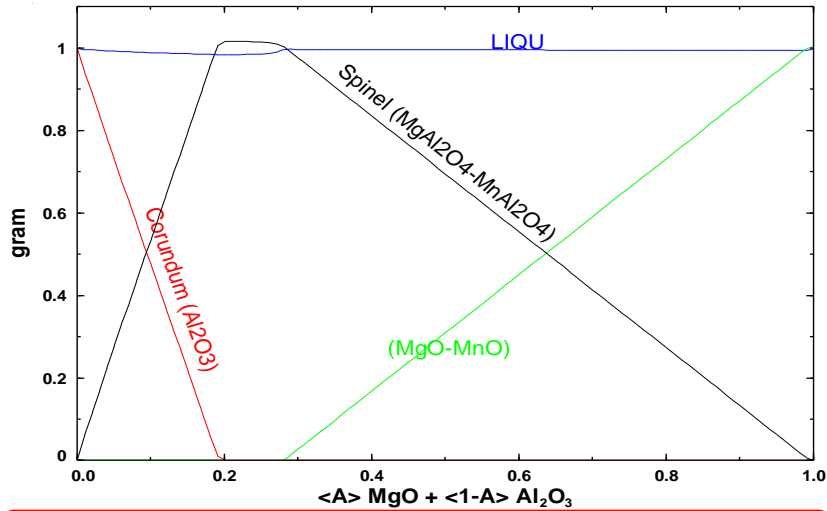


1g Mn-Fe melt + 1g refractor



High Mn-Fe melt storage for TWIP Steel production

1g Mn-Fe melt + 1g refractory (MgO-Al₂O₃)

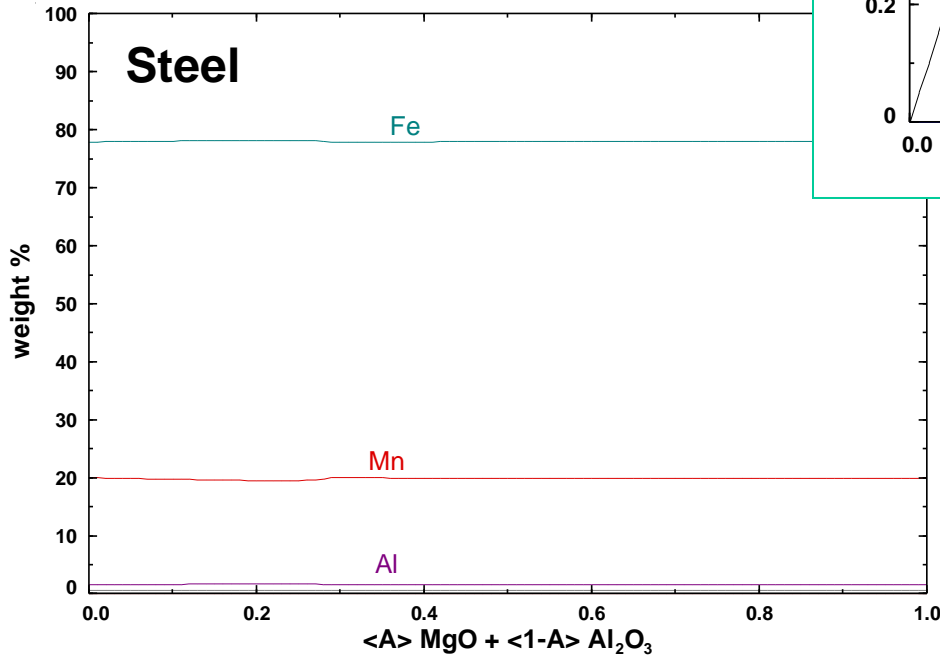
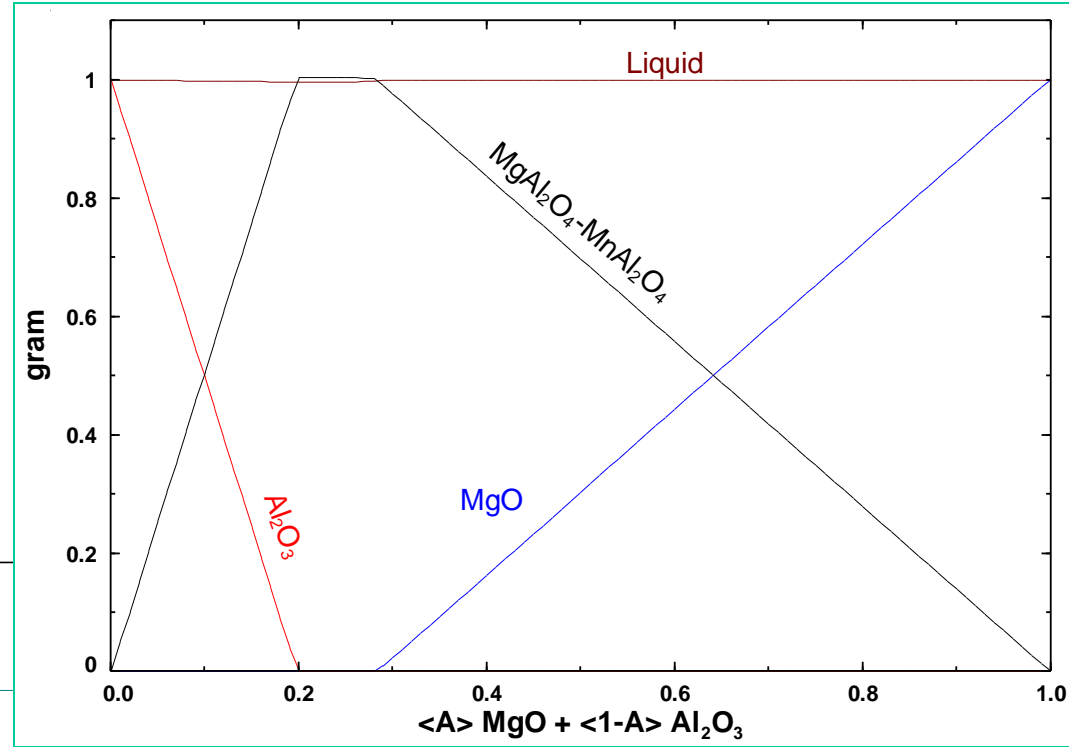
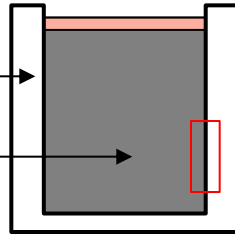


Refractory for TWIP steel: Fe-20%Mn-1.5%Al-0.6%C

T = 1500°C

Refractories

Twip steel



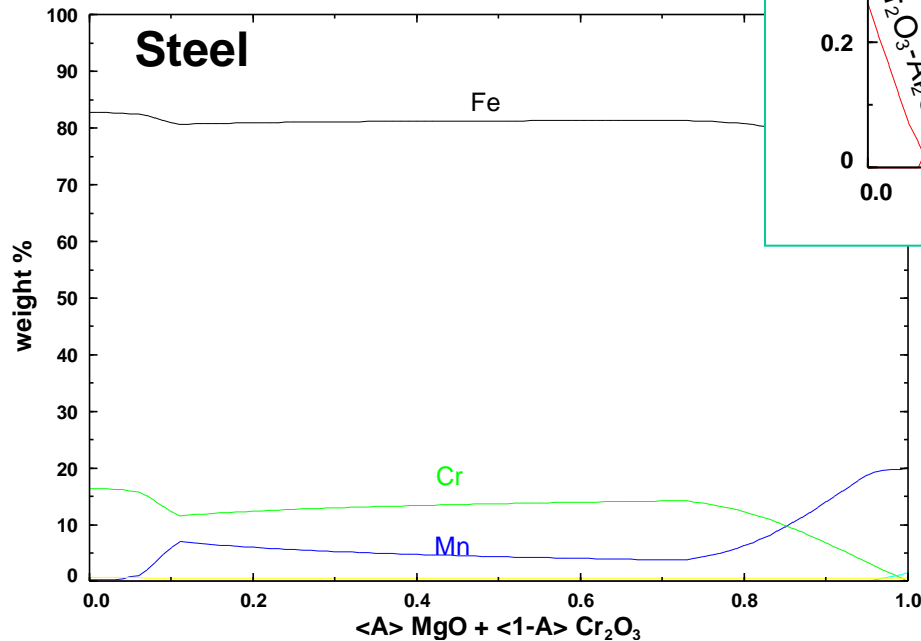
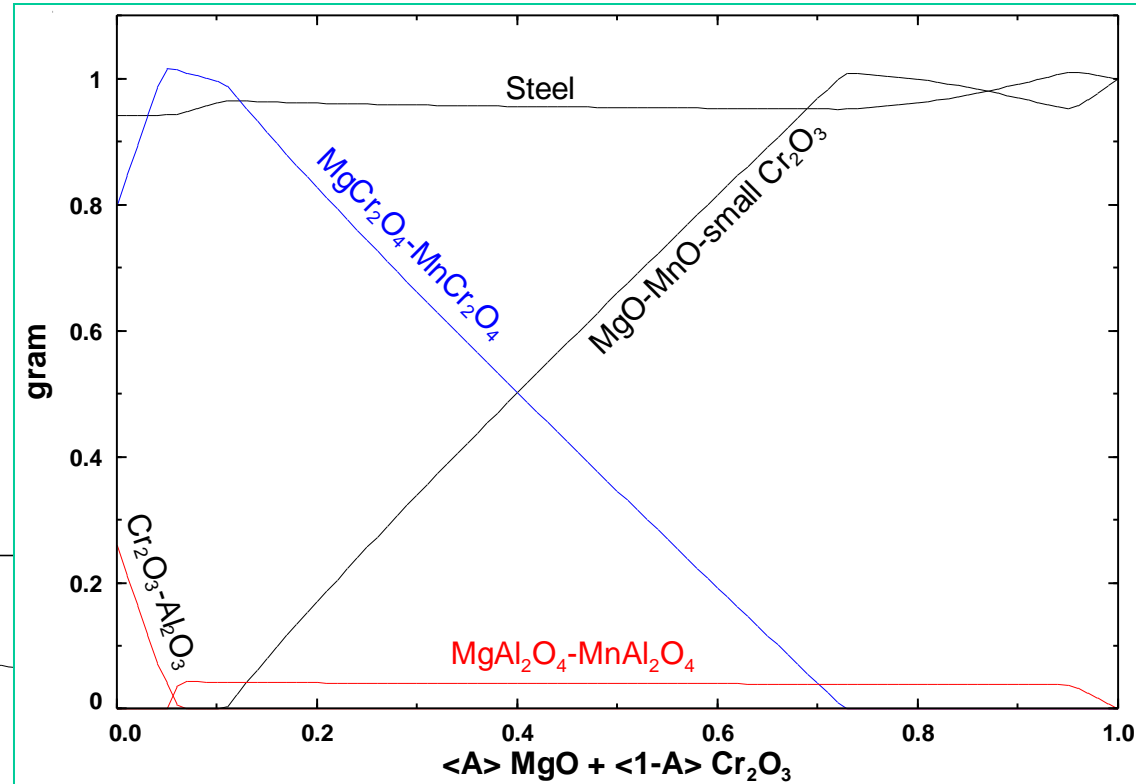
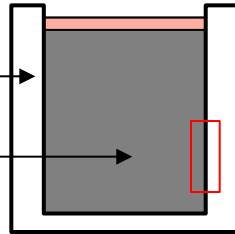
MgO-Al₂O₃ type: Very stable refractory

Refractory for TWIP steel: Fe-20%Mn-1.5%Al-0.6%C

T = 1500°C

Refractories

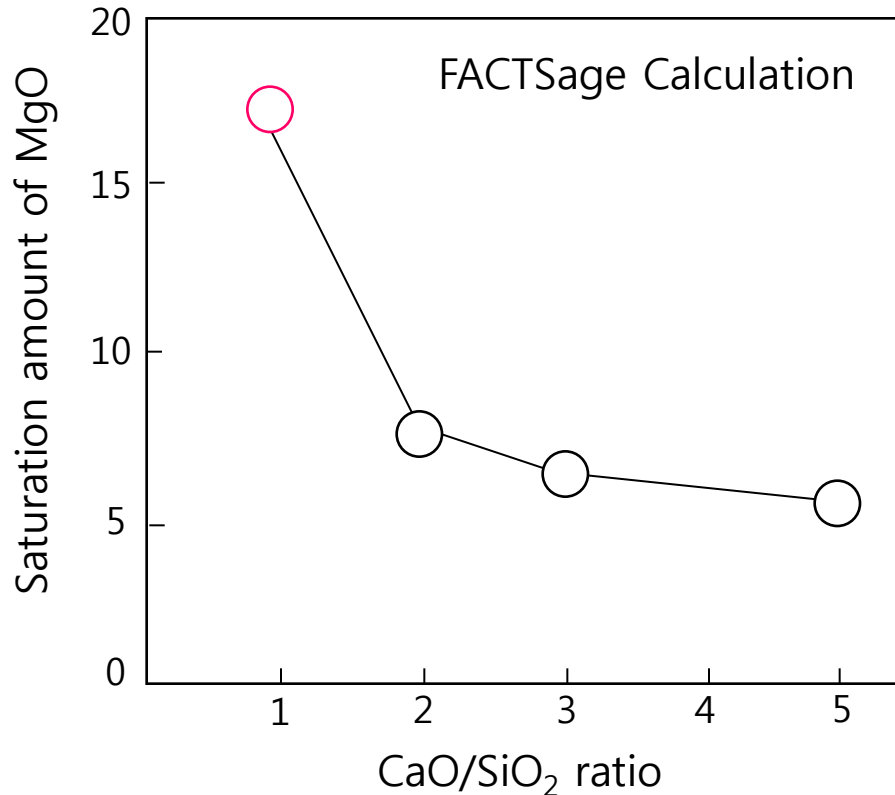
Twip steel



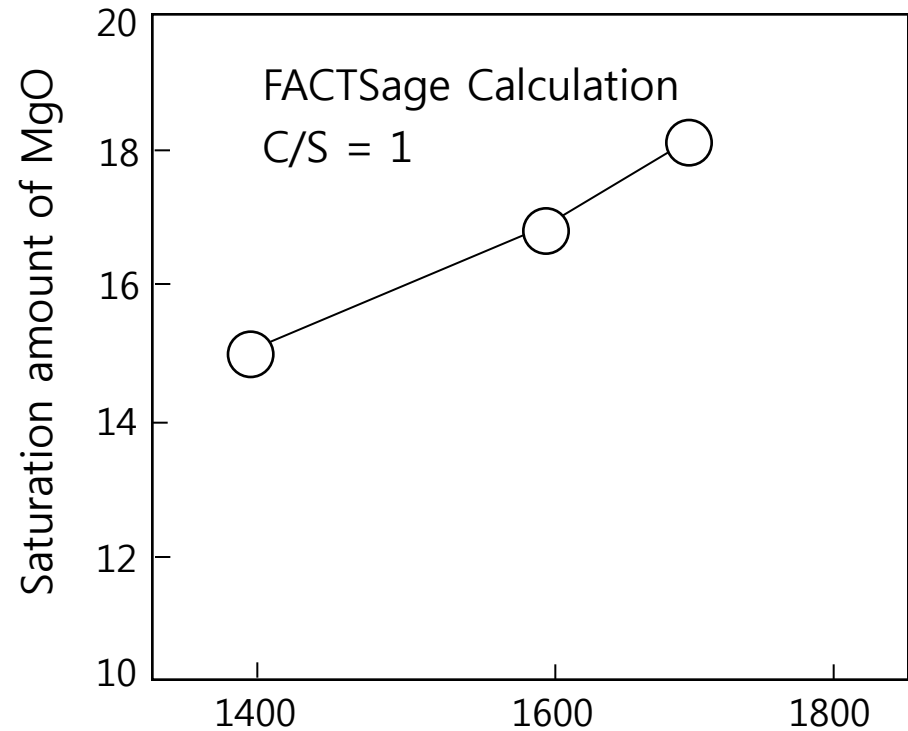
MgO-Cr₂O₃ type: less stable
 → Cr pickup
 → Al loss

Refining slag for High Mn Steel

- Slag : MnO 20~50%, CaO-SiO₂ system
- Refractory : MgO-C (C=18%)
- **Variants: Slag basicity, FeO/MnO content, and temperature**

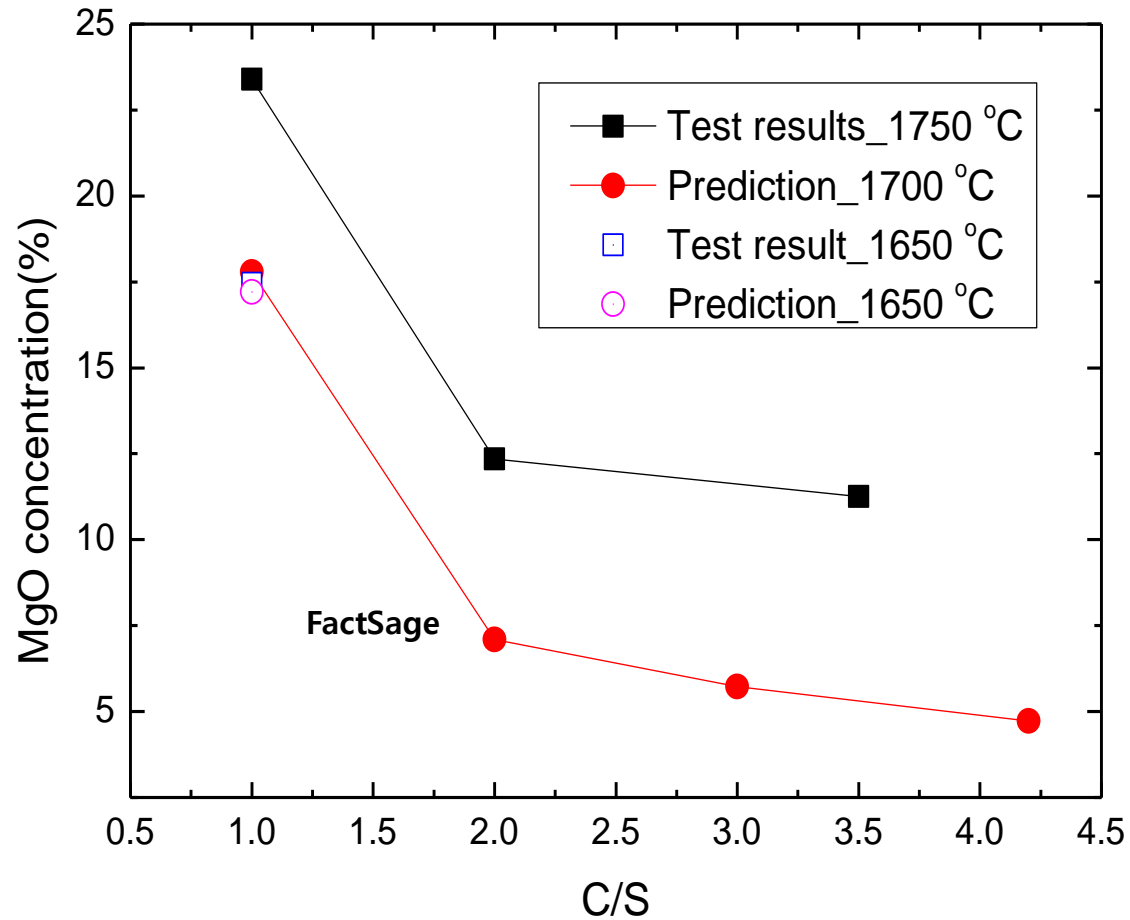


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Experimental MgO solubility vs. calculated results from FactSage



Development of a kinetic model for the RH process

Marie-Aline Van Ende and In-Ho Jung



Dept. Mining and Materials Engineering
McGill University



Van Ende et al: 'A Kinetic Model for the Ruhrstahl Heraeus (RH) Degassing Process', Metall. Mater. Trans. B, 2011, p. 477

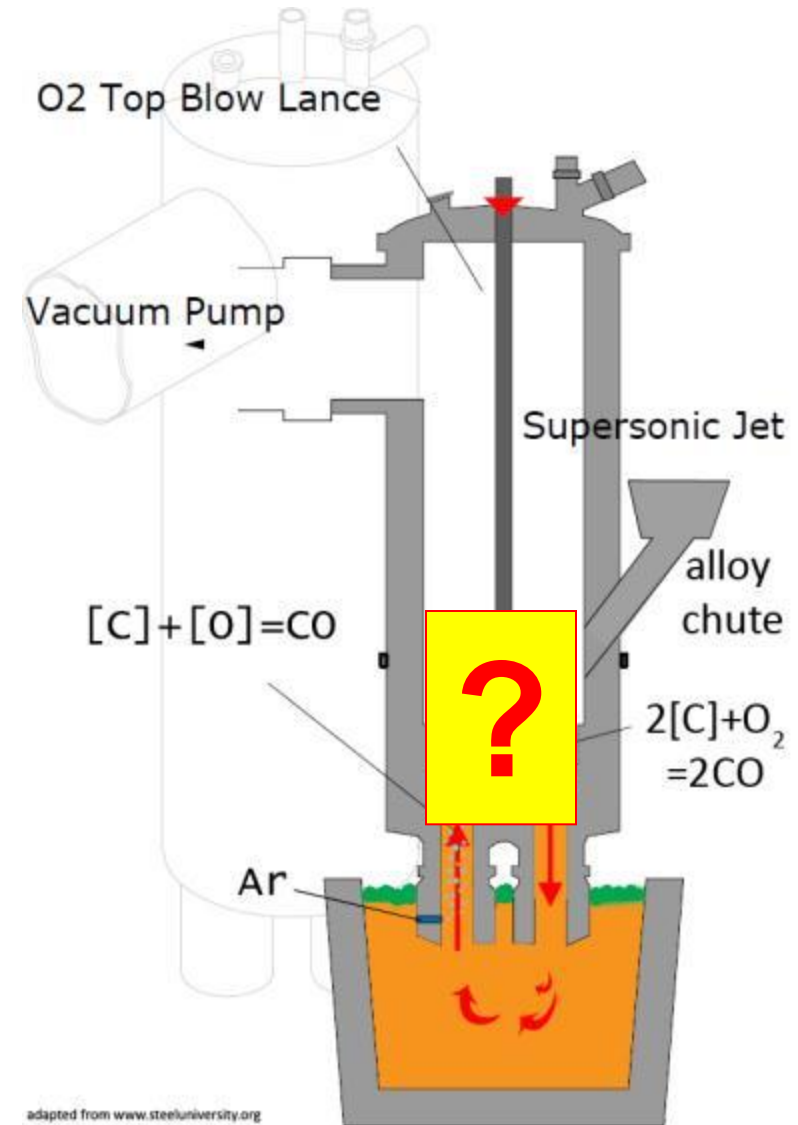
Operations in recirculation RH degasser

- Pair of snorkel lowered into liquid steel
- Vessel pressure lowered to ~1 torr
- Ar injected in one of the snorkel \Rightarrow steel up into the unit and out again through the other snorkel
- O₂ injected through a top lance
- Addition of alloys



http://www.aksteel.com/production_facilities/fac_pop_ash.html

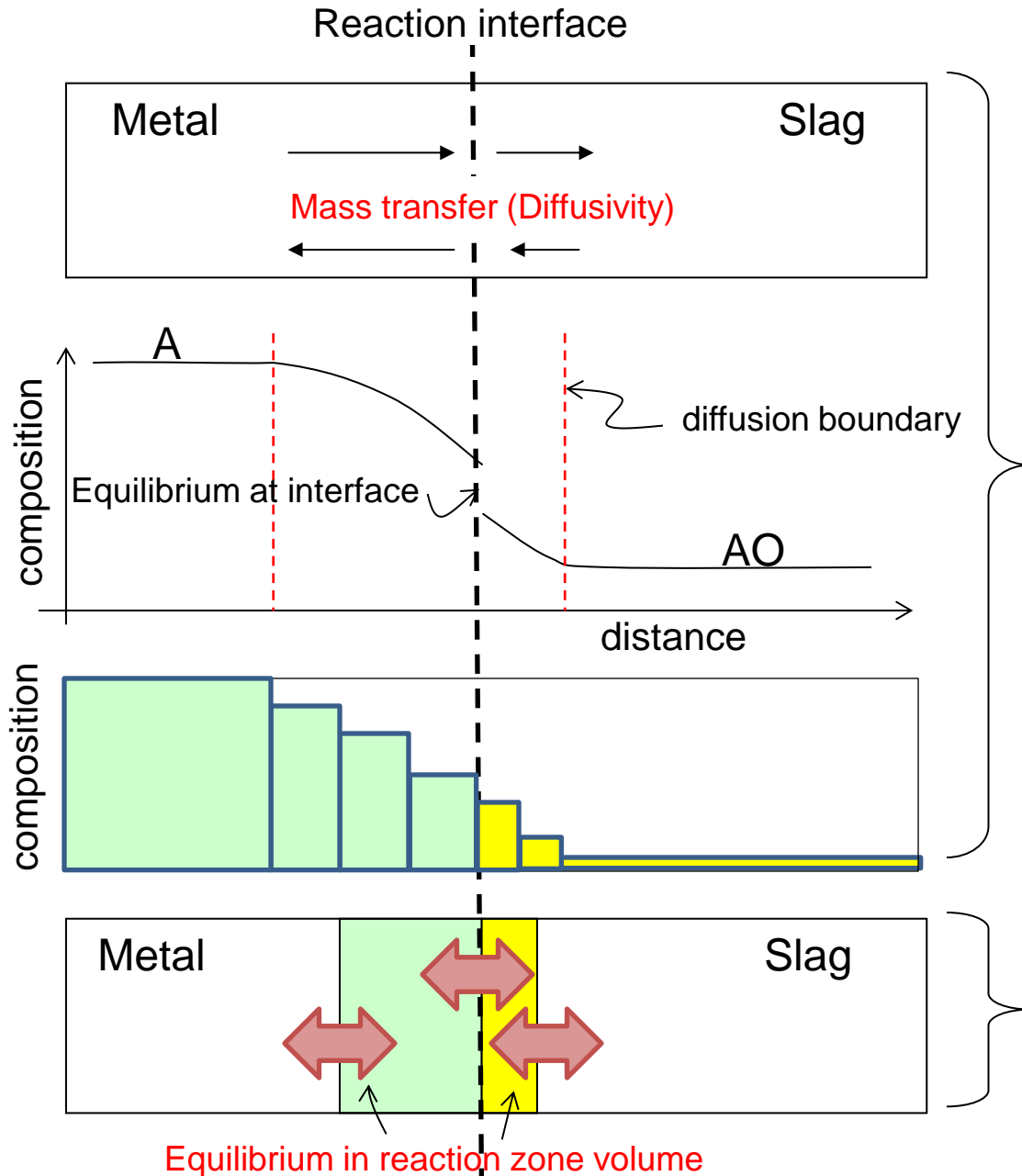
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adapted from www.steeluniversity.org

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Effective Equilibrium Reaction Zone model



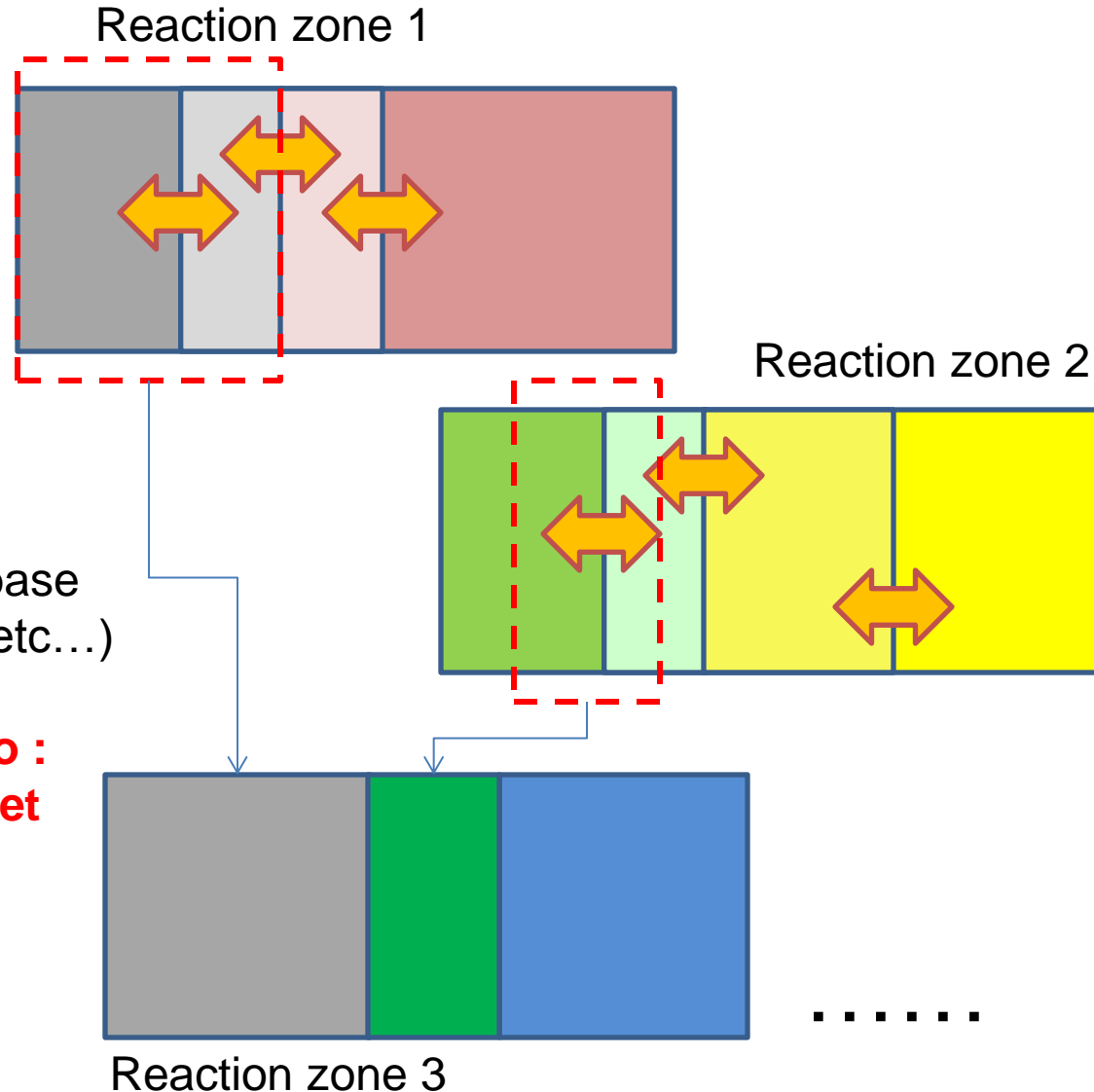
Real Process

- Very complex
- Difficult to find diffusivities
- Case by Case

Reaction Zone Model

- Simple
- Easy to find by experiment

Concept for process simulation modeling



Quite enough thermodynamic database
(gas, molten steel, slag, refractory, etc...)

**Write kinetic process using Macro :
input/output to Excel spread sheet**

Heat & Mass balance !!
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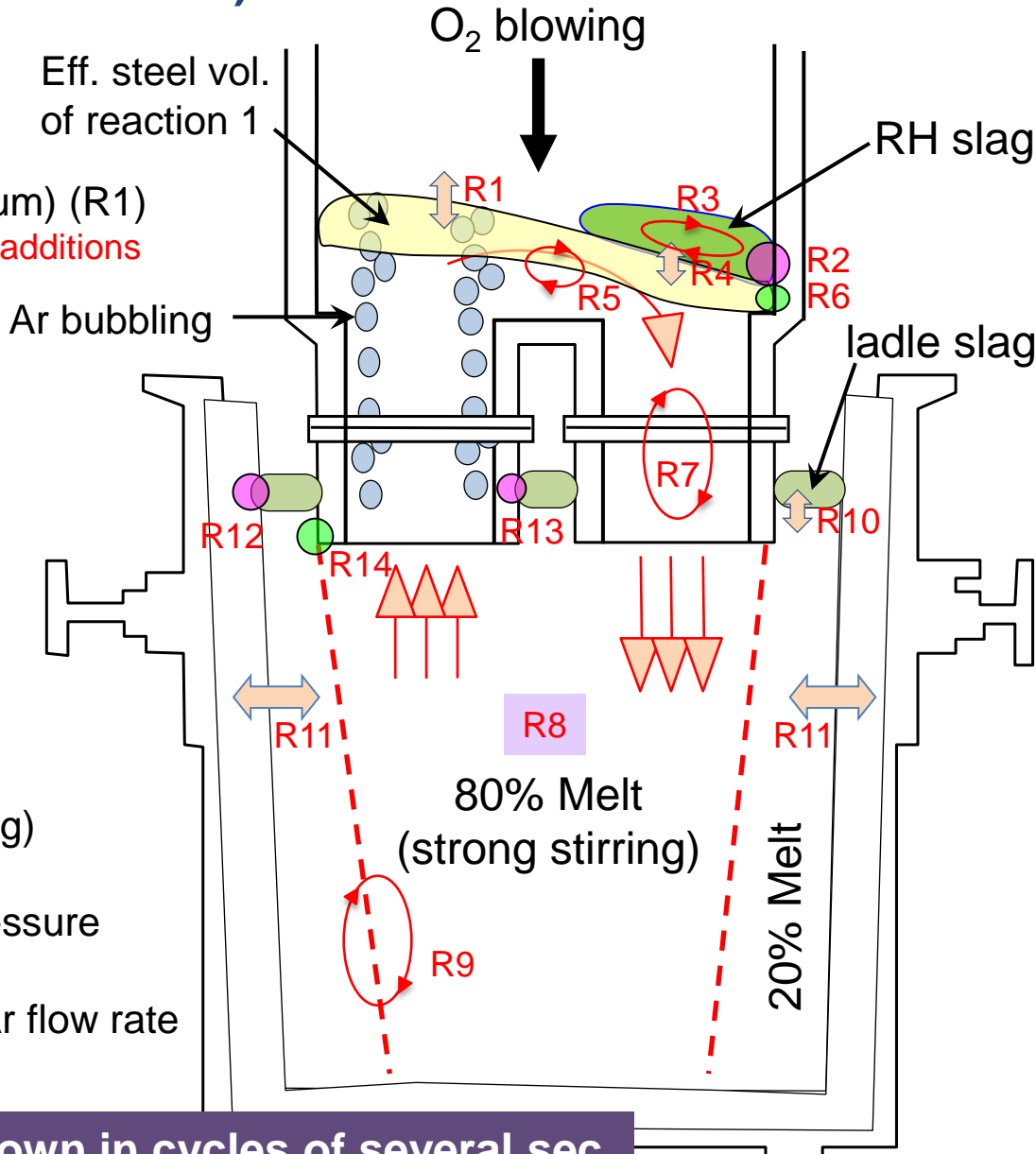
RH process model (3rd generation model)

9 reaction zones:

- RH steel + RH atmosphere (O_2 or vacuum) (R1)
effective steel volume + X% O_2 + vacuum + additions
- RH slag + RH refractory (R2)
- RH slag mixing (R3)
- RH steel + RH slag (R4)
- First mixing in RH (R5)
- RH steel + RH refractory (R6)
- Second mixing in RH (R7)
- Mixing in ladle circulation zone (R8)
- Homogenization in ladle (R9)

Main assumptions:

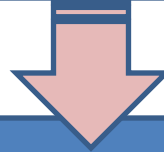
- RH steel capacity: 21 ton
- Initial RH slag amount: 260 kg (ladle slag)
- Adiabatic heat condition (no heat loss)
- Limited steel exposure to RH vessel pressure
- RH refractory: pure $MgO.Cr_2O_3$
- RH circulation force dependent on the Ar flow rate and on the RH vessel pressure



⇒ The RH process is broken down in cycles of several sec

How to determine the reaction volumes?

Physical description of the reaction kinetics



- Mathematical expressions (literature)
- Empirical relations (plant data, lab experiments, etc.)
- Fitting parameters



Mathematical expressions of the effective reactions zone volumes as a function of the process conditions

Macro processing

RH treatment duration: ~25 min \Rightarrow ~300 cycles * 9 reactions

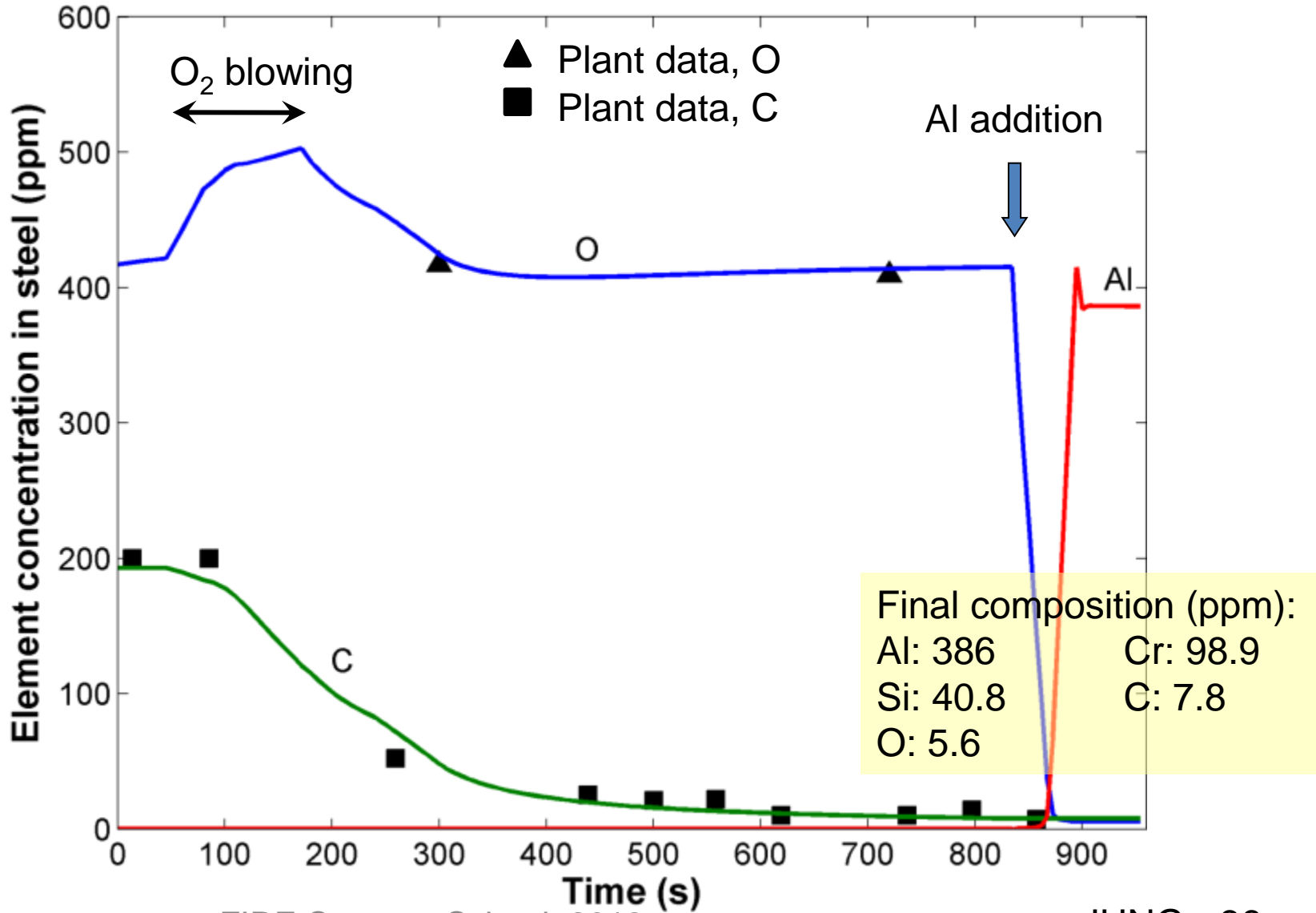
~ **2700 Equilib runs!**



Macro processing is a powerful tool to deal with such complex process

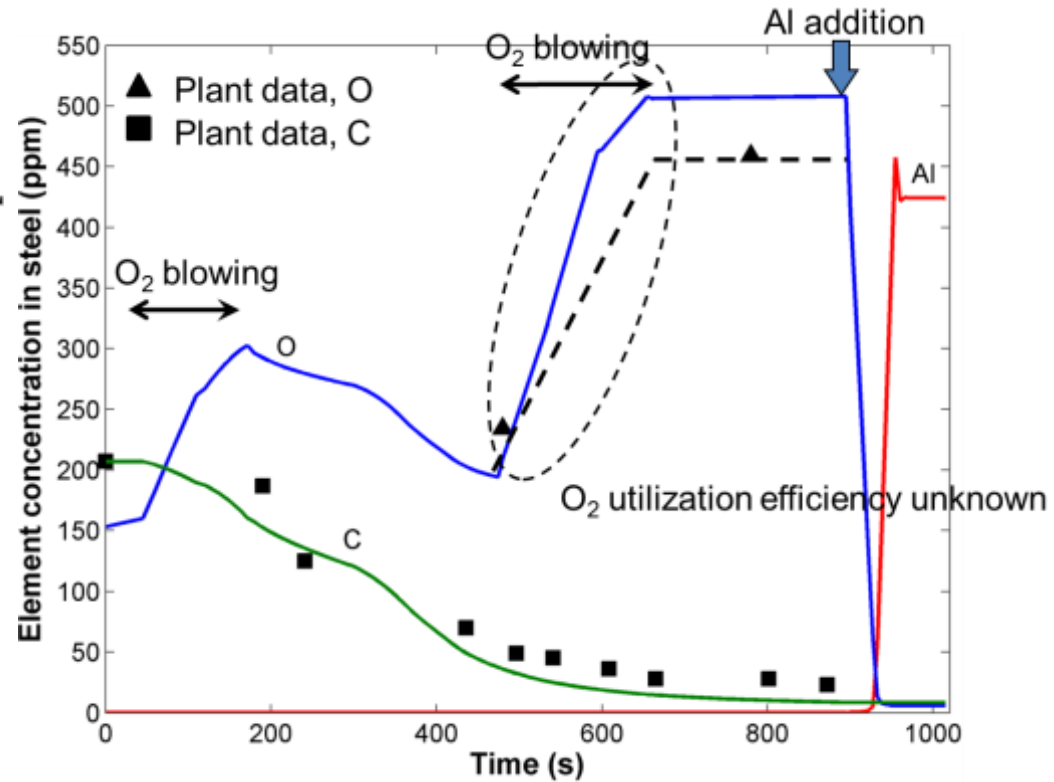
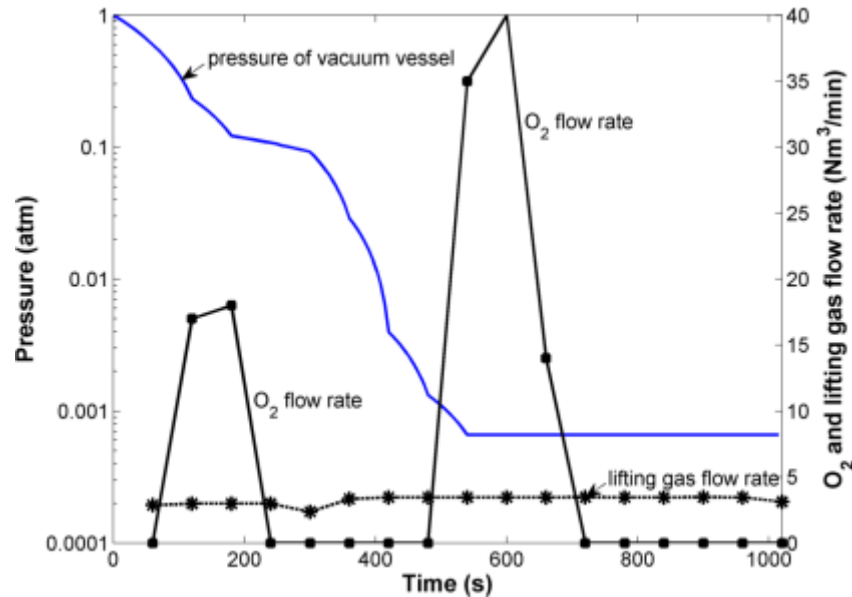
- Run Equilib files for each reaction automatically
- Handle all streams between each cycle
- Read the input and store the results in Excel spreadsheets

Evolution of ladle steel composition



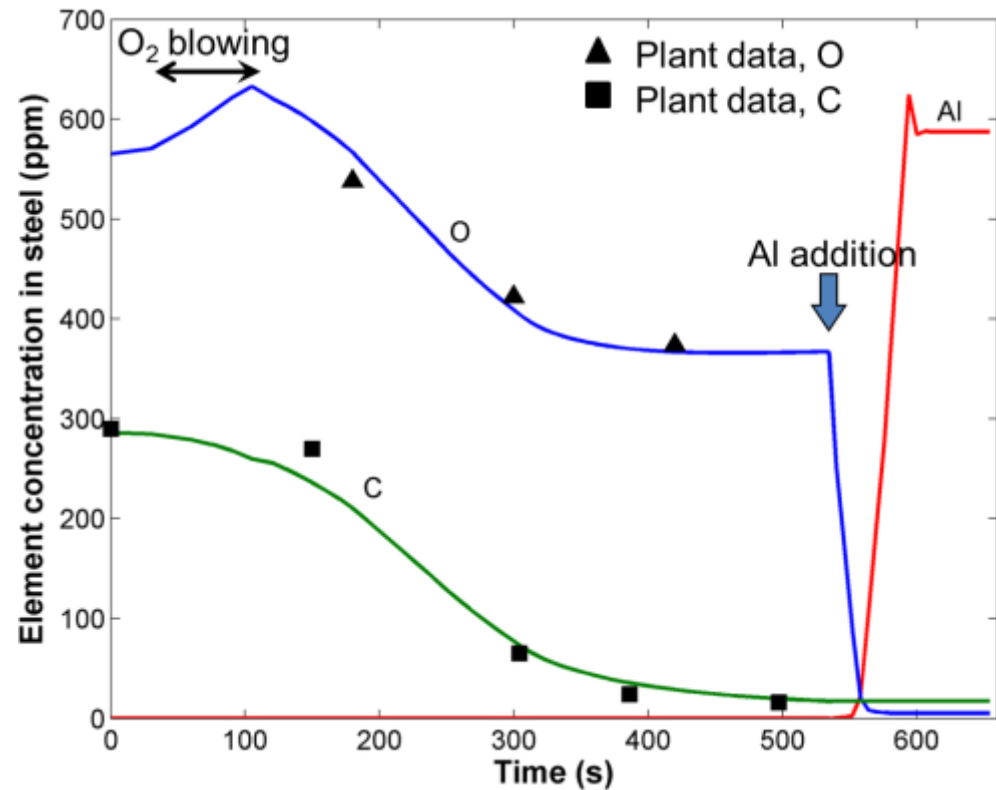
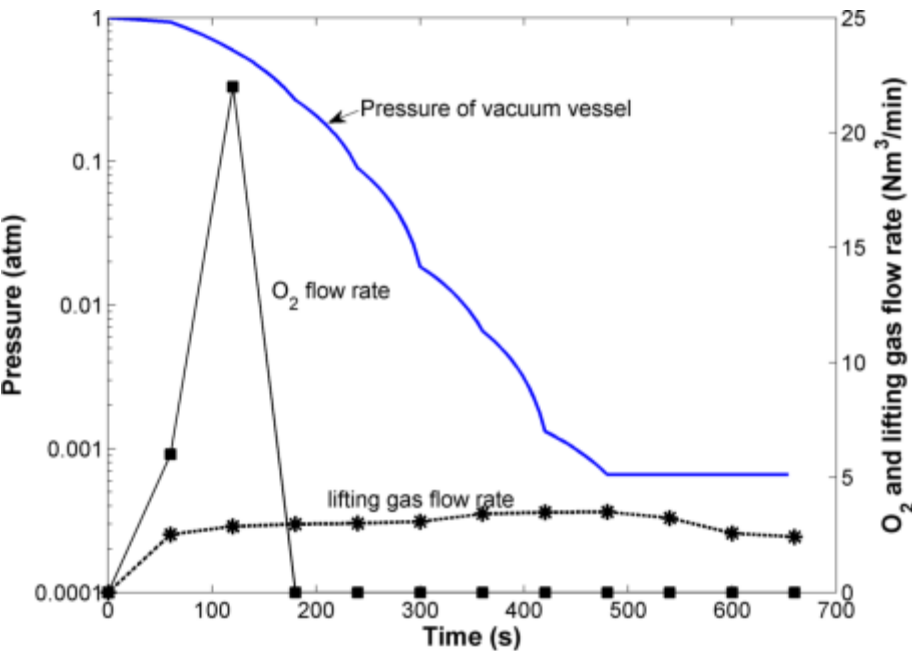
Application to extreme process conditions

Case 1: low O content

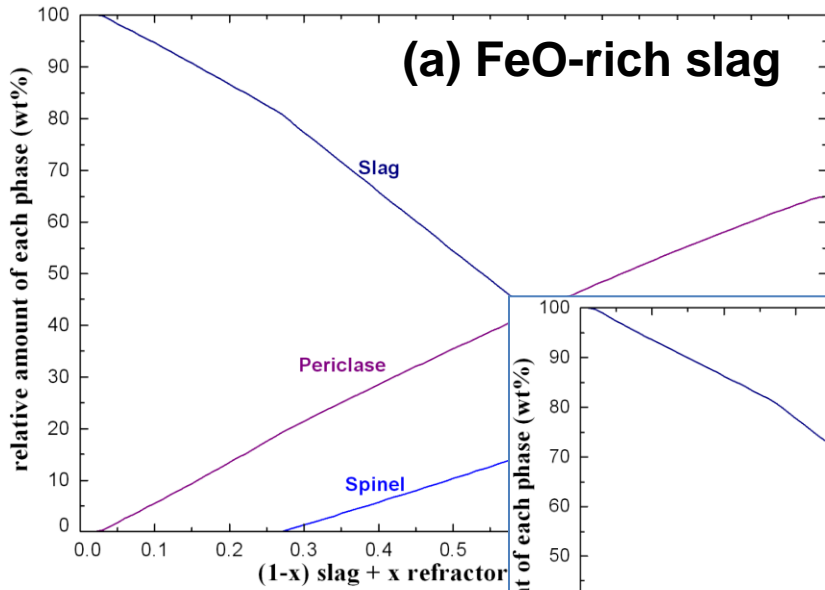


Application to extreme process conditions

Case 2: high O content



Corrosion of RH Vessel Refractory by RH slags



Magnesia-Chromite refractory
(57.0 MgO, 23.4 Cr₂O₃, 8.4 Al₂O₃, 11.2 wt% FeO)
65wt% periclase (MgO-FeO-Cr₂O₃) + 35 wt% spinel

